

Seventh Framework Programme<br>Marie Curie Action 'International Research Staff Exchange Scheme"<br>Paton Welding Institute<br>Kiev, Ukraine

## Protocols of static internal pressure test of specimens I1, I2, I3 and I4 made of pipe 219×6 (Steel 20)

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## Data common to specimens I1 ... I4.

Table 1. Results of tensile testing of specimens from the pipe $219 \times 6$ material (steel 20), cut in the circumferential and axial direction in the state of delivery (tension up to formation the neck in the working portion of the specimen).

| measurement \# | Direction of the specimen |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | circumferential |  | axial |  |
|  | strain | stress | strain | stress |
|  | e | $\sigma, \mathrm{MPa}$ | e | $\sigma, \mathrm{MPa}$ |
| 1 | 2 | 3 | 4 | 5 |
| 1 | 0 | 0 | 0 | 0 |
| 2 | 3.26E-05 | 8 | 0.000151 | 19.98938 |
| 3 | 0.000106 | 24.0249 | 0.000185 | 29.54951 |
| 4 | 0.000144 | 29.18004 | 0.000215 | 38.62682 |
| 5 | 0.000162 | 34.33518 | 0.00025 | 48.38009 |
| 6 | 0.000192 | 39.19852 | 0.000293 | 58.42306 |
| 7 | 0.000218 | 43.96459 | 0.000336 | 67.88663 |
| 8 | 0.000239 | 48.6334 | 0.000384 | 78.02617 |
| 9 | 0.000252 | 53.69128 | 0.000436 | 87.29661 |
| 10 | 0.000269 | 58.74915 | 0.00047 | 96.56704 |
| 11 | 0.000278 | 62.83435 | 0.000531 | 106.3203 |
| 12 | 0.000308 | 67.79496 | 0.000608 | 116.653 |
| 13 | 0.000338 | 73.5337 | 0.000652 | 125.5372 |
| 14 | 0.000347 | 78.20251 | 0.000708 | 135.7733 |
| 15 | 0.000368 | 82.19045 | 0.000755 | 145.43 |
| 16 | 0.000398 | 87.63739 | 0.000816 | 154.4107 |
| 17 | 0.000415 | 92.598 | 0.000885 | 164.2605 |
| 18 | 0.00045 | 97.75314 | 0.000932 | 174.3035 |
| 19 | 0.000476 | 102.0329 | 0.001002 | 183.6705 |
| 20 | 0.000471 | 106.7017 | 0.001066 | 192.9409 |
| 21 | 0.000527 | 112.635 | 0.001148 | 203.2736 |
| 22 | 0.00054 | 116.5256 | 0.001205 | 212.7372 |
| 23 | 0.00057 | 122.2644 | 0.001313 | 222.7802 |
| 24 | 0.000587 | 126.7386 | 0.001421 | 232.5334 |
| 25 | 0.000648 | 137.0489 | 0.001511 | 241.9004 |
| 26 | 0.000695 | 146.0947 | 0.001667 | 251.4606 |
| 27 | 0.000759 | 155.4324 | 0.001831 | 260.9241 |
| 28 | 0.00082 | 165.6454 | 0.001973 | 271.0637 |
| 29 | 0.000876 | 175.372 | 0.002198 | 280.141 |
| 30 | 0.000944 | 185.5851 | 0.002453 | 289.7977 |
| 31 | 0.001005 | 194.6309 | 0.002552 | 294.0466 |

Table 1 (continued)

| 1 | 2 | 3 |  | 4 |
| :---: | :---: | :---: | :---: | :---: |
|  | 22 | 5 |  |  |
| 32 | 0.001065 | 204.0658 | 0.002729 | 299.8407 |
| 33 | 0.001151 | 214.6678 | 0.002889 | 304.1862 |
| 34 | 0.001228 | 223.6164 | 0.003183 | 309.3042 |
| 35 | 0.001336 | 233.1485 | 0.003351 | 313.4566 |
| 36 | 0.001452 | 243.2643 | 0.003589 | 313.9395 |
| 37 | 0.001602 | 252.8937 | 0.003874 | 316.933 |
| 38 | 0.001805 | 263.204 | 0.004181 | 317.0296 |
| 39 | 0.00205 | 272.5416 | 0.004583 | 318.285 |
| 40 | 0.002355 | 282.0737 | 0.005066 | 318.7678 |
| 41 | 0.002794 | 292.0922 | 0.006237 | 319.0575 |
| 42 | 0.003314 | 301.5271 | 0.006656 | 317.9953 |
| 43 | 0.003921 | 311.4483 | 0.00819 | 320.6026 |
| 44 | 0.004725 | 320.8832 | 0.011499 | 320.8923 |
| 45 | 0.005757 | 330.9017 | 0.015542 | 323.6927 |
| 46 | 0.007193 | 340.4338 | 0.017745 | 324.755 |
| 47 | 0.009408 | 350.6468 | 0.020838 | 328.7142 |
| 48 | 0.011533 | 359.8872 | 0.022587 | 331.9009 |
| 49 | 0.01444 | 369.7111 | 0.024453 | 335.7636 |
| 50 | 0.017718 | 379.5351 | 0.026272 | 340.9782 |
| 51 | 0.021524 | 388.9699 | 0.029499 | 348.607 |
| 52 | 0.026328 | 399.183 | 0.032933 | 357.2981 |
| 53 | 0.03228 | 408.5206 | 0.036134 | 364.8303 |
| 54 | 0.039015 | 418.5391 | 0.039469 | 372.7488 |
| 55 | 0.047381 | 428.2657 | 0.042907 | 379.605 |
| 56 | 0.058571 | 437.8951 | 0.046303 | 383.7574 |
| 57 | 0.073362 | 447.6218 | 0.049823 | 389.648 |
| 58 | 0.080588 | 452.3879 | 0.053223 | 395.1523 |
| 59 | 0.091503 | 457.154 | 0.056679 | 399.7876 |
| 60 | 0.097529 | 460.072 | 0.060117 | 404.1331 |
| 61 | 0.105741 | 462.0173 | 0.063465 | 407.6095 |
| 62 | 0.108982 | 462.99 | 0.066908 | 412.4378 |
| 63 | 0.117461 | 465.908 | 0.070454 | 416.0108 |
| 64 | 0.124447 | 468.0479 | 0.074001 | 418.6181 |
| 65 | 0.130565 | 469.2151 | 0.077547 | 422.4808 |
| 66 | 0.14166 | 470.8686 | 0.080865 | 425.4744 |
| 67 | 0.147745 | 471.8413 | 0.084342 | 428.0817 |
| 68 | 0.156018 | 472.3276 | 0.087906 | 430.4959 |
| 69 | 0.162021 | 473.4948 | 0.091496 | 433.1032 |
| 70 | 0.166767 | 473.6893 | 0.095129 | 434.938 |
| 71 | 0.170957 | 474.1757 | 0.09874 | 437.4487 |
| 72 | 0.176682 | 474.3702 | 0.100277 | 438.5109 |
| 73 | 0.182505 | 474.5647 | 0.103498 | 438.9938 |
|  |  |  |  |  |
| 4 |  |  |  |  |

Table 1 (continued)

| 1 | 2 | 3 | 4 | 5 |
| :---: | :---: | :---: | :---: | :---: |
| 74 | 0.18944 | 474.7593 | 0.107119 | 441.9873 |
| 75 | 0.195191 | 474.1757 | 0.110619 | 442.3736 |
| 76 | 0.200817 | 474.7593 | 0.113921 | 443.7256 |
| 77 |  |  | 0.117327 | 445.6569 |
| 78 |  |  | 0.120642 | 447.1054 |
| 79 |  |  | 0.124086 | 448.4573 |
| 80 |  |  | 0.127466 | 450.9681 |
| 81 |  |  | 0.131035 | 450.6784 |
| 82 |  |  | 0.134522 | 452.1269 |
| 83 |  |  | 0.138117 | 454.0582 |
| 84 |  |  | 0.141712 | 454.0582 |
| 85 |  |  | 0.145332 | 454.4445 |
| 86 |  |  | 0.148975 | 455.4102 |
| 87 |  |  | 0.152737 | 456.7621 |
| 88 |  |  | 0.156409 | 457.1484 |
| 89 |  |  | 0.16015 | 458.6934 |
| 90 |  |  | 0.163857 | 458.5969 |
| 91 |  |  | 0.167697 | 459.9488 |
| 92 |  |  | 0.171201 | 459.3694 |
| 93 |  |  | 0.175067 | 459.466 |
| 94 |  |  | 0.178881 | 459.7557 |
| 95 |  |  | 0.182759 | 460.142 |
| 96 |  |  | 0.186672 | 460.9145 |
| 97 |  |  | 0.190461 | 460.6248 |
| 98 |  |  | 0.19409 | 461.3008 |
| 99 |  |  | 0.198306 | 460.142 |
| 100 |  |  | 0.201531 | 460.9145 |
| 101 |  |  | 0.20485 | 460.2385 |
| 102 |  |  | 0.208101 | 460.6248 |
| 103 |  |  | 0.211481 | 461.3973 |
| 104 |  |  | 0.214718 | 460.8179 |
| 105 |  |  | 0.217873 | 461.1076 |
| 106 |  |  | 0.221137 | 460.0454 |
| 107 |  |  | 0.2244 | 461.3973 |
| 108 |  |  | 0.227659 | 461.0111 |
| 109 |  |  | 0.230819 | 460.9145 |
|  |  |  |  |  |
| 7 |  |  |  |  |
| 9 |  |  |  |  |
| 9 |  |  |  |  |
| 9 |  |  |  |  |



Fig. 1. Schemes of specimens I1 ... I4 wall thickness measurement (sweep of the cylindrical part): a - location of perimeter measurement sections I, II, III; b-location of the punching points 1* ..16* in sections I, II, III, $1 \ldots 16$ - point of wall thickness measurement; c - wall thickness measurement in defects of specimens I2, I3. (Dimensions in mm).

Measuring of the wall thickness and perimeter of specimens I2 and I3 (with defect) was done only in sections I * and II *.

For the perimeter determination was used tape line with thickness of 0.2 mm . The wall thickness of cylindrical portion of the specimens was measured by ultrasonic thickness gauge TUZ-2.

Two end plates were used for specimen hermetic sealing (Fig. 2).


Fig. 2. Steel plates for specimens I1 ... I 4 sealing. (Dimensions in mm).

## HYDRAULIC PRESSURE TESTS

## Protocol of specimen I1 (without defect).

For the manufacture of the specimen was used piece of pipe \#8, weight 33.2 kgf (Fig.3a). Sections I, II, III had punched points (marked with "*" on Fig.1). Distance between points was used as the base for measuring residual deformation in circumferential and axial direction before and after destruction (Fig 1b, Table.2, 4).

Table 2. Length of cylindrical portion of specimen I1 and base axial dimensions in the original state.

| $\#$ | Linear size, mm | Sector |  |  |  |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
|  |  | I | II | III | IV | average |
| 1 | length of the pipe piece, $1_{o}$ | 949 | 949 | 946 | 946 | 947.5 |
| 2 | length between the inner surfaces of the plates <br> (bottoms) after welding | 954 | 954 | 952 | 952 | 953 |
| 3 | distance between the sections I-III | 646.5 | 646.5 | 645 | 644 |  |
| 4 | distance between the sections I-II | 325 | 325 | 324 | 323 |  |
| 5 | distance between the sections II-III | 321.5 | 321.5 | 321 | 321 |  |
| D |  |  |  |  |  |  |

Dimensions 3, 4, 5, after the destruction of the specimen did not change, indicating the absence of residual deformation in the axial direction.
Note: The measurements were done in the middle of the sectors I ... IV, (Fig. 1). The distance between the cross sections was determined by the punching points.

Table 3. Specimen I1 perimeter before $\left(\mathrm{P}_{\mathrm{H}}\right)$ and after destruction $\left(\mathrm{P}_{\mathrm{K}}\right)$.

| Cross section $\rightarrow$ | I (150 mm from the <br> top) | II (in the middle) | III (150 mm from <br> the bottom) | average |
| :---: | :---: | :---: | :---: | :---: |
| Perimeter, $\mathrm{P}_{\mathrm{H}}, \mathrm{mm}$ | 693.5 | 693.5 | 693.5 | 693.5 |
| Perimeter, $\mathrm{P}_{\mathrm{K}}, \mathrm{mm}$ | 744 | 753 | 741 | 746 |

Table 4. Specimen I1. Base length and the wall thickness in the sections I, II, III before ( $l_{\mathrm{H}}, \mathrm{s}_{\mathrm{H}}$ ) and after destruction $\left(l_{K}, \mathrm{~s}_{\mathrm{K}}\right),(\mathrm{mm})$.

| Distance | Measuring point \# | Sec. I |  | Sec. I |  | Sec. II |  | Sec. II |  | Sec. III |  | Sec. III |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{l}_{\mathrm{H}}$ | $\mathrm{S}_{\mathrm{H}}$ | $1_{K}$ | $\mathrm{S}_{\mathrm{K}}$ | $\mathrm{l}_{\mathrm{H}}$ | $\mathrm{S}_{\mathrm{H}}$ | $\mathrm{l}_{\mathrm{K}}$ | $\mathrm{S}_{\mathrm{K}}$ | $\mathrm{l}_{\mathrm{H}}$ | $\mathrm{S}_{\mathrm{H}}$ | $\mathrm{l}_{\mathrm{K}}$ | $\mathrm{S}_{\mathrm{K}}$ |
| $1^{*}-2^{*}$ | 1 | 43.2 | 6.7 | 46.1 | 6.3 | 46.2 | 6.5 | 51.4 | 5.8 | 42 | 6.8 | 44.8 | 6.4 |
| $2^{*}-3^{*}$ | 2 | 43.7 | 6.2 | 48.4 | 5.7 | 44 | 6.3 | 51.2 | 5.5 | 42.4 | 6.6 | 45.3 | 6.2 |
| 3*-4* | 3 | 44 | 6.0 | 51 | 5.1 | 44.5 | 6.3 | - | 5.4 | 43.2 | 6.6 | 46.4 | 6.0 |
| $4^{*}-5^{*}$ | 4 | 41.6 | 6.2 | 46.3 | 5.6 | 44.5 | 6.2 | 51.5 | 5.2 | 44.5 | 6.5 | 47.8 | 5.9 |
| $5^{*}-6^{*}$ | 5 | 42.6 | 6.2 | 46.8 | 5.8 | 42.8 | 6.5 | 47 | 5.9 | 43.2 | 6.2 | 48 | 5.6 |
| $6^{*}-7{ }^{*}$ | 6 | 44 | 6.5 | 47.1 | 6.0 | 41.7 | 6.4 | 46.8 | 5.6 | 42.6 | 6.3 | 47 | 5.7 |
| $7^{*}-8^{*}$ | 7 | 43 | 6.6 | 46 | 6.1 | 43 | 6.8 | 47.2 | 6.1 | 42.1 | 6.2 | 46.2 | 5.7 |
| $8^{*}-9^{*}$ | 8 | 45.5 | 6.9 | 48.2 | 6.5 | 40.8 | 6.8 | 43.6 | 6.4 | 44 | 6.7 | 47 | 6.2 |
| $9^{*}-10^{*}$ | 9 | 43 | 7.2 | 45 | 6.9 | 43.5 | 7.1 | 45.8 | 6.8 | 42.8 | 7.2 | 45 | 6.8 |
| $10^{*}-11^{*}$ | 10 | 42.8 | 7.4 | 44.2 | 7.1 | 42.8 | 7.4 | 44.6 | 7.1 | 42.4 | 7.1 | 44 | 6.9 |
| $11^{*}-12^{*}$ | 11 | 44 | 7.4 | 45.8 | 7.2 | 43.7 | 7.1 | 45.5 | 6.9 | 43 | 6.9 | 45 | 6.6 |
| $12^{*}-13^{*}$ | 12 | 41.5 | 7.2 | 43.2 | 6.9 | 41.6 | 6.9 | 44 | 6.6 | 43.5 | 6.9 | 45.4 | 6.5 |
| 13**** | 13 | 44.3 | 6.8 | 46.8 | 6.5 | 42 | 6.7 | 45 | 6.6 | 43.8 | 6.9 | 46 | 6.6 |
| $14^{*}-15^{*}$ | 14 | 42.7 | 6.5 | 45.5 | 6.2 | 44 | 6.7 | 47 | 6.4 | 43.4 | 7.0 | 45.4 | 6.6 |
| $15^{*}-16^{*}$ | 15 | 43 | 6.7 | 46 | 6.2 | 42.4 | 6.9 | 45.4 | 6.8 | 44.8 | 6.9 | 47.2 | 6.7 |
| $16^{*}-1^{*}$ | 16 | 42.8 | 6.8 | 45.3 | 6.4 | 44.4 | 6.8 | 47.2 | 6.5 | 43.4 | 6.8 | 46 | 6.3 |
| $\Sigma$ | - | 691.7 | - | 741.7 | - | 691.9 | - | 703.2 | - | 691.1 | - | 736.5 | - |
| average | - | 43.23 | 6.71 | 46.36 | 6.28 | 43.24 | 6.71 | 46.88 | 6.23 | 43.19 | 6.73 | 46.03 | 6.29 |

Weight of welded specimen: 61.2 kg . Weight of the specimen filled with water: 93.2 kg . Water temperature: $18^{\circ} \mathrm{C}$. Water weight: 32 kg . Internal volume of the specimen 32 liters.


Fig. 3. Specimen I1 (points indicate places of the measurement thickness): a - pipe piece \#8; b specimen before the test; c - welding of the pipe; d - top bottom with the fittings.

Results of measuring of wall thickness of the sample before and after the test are given at Fig. 4 and Fig.5, correspondingly.

| Thickness in original state |  |  |  |  |  |  |  |  |  |  |  |  |  | sample |  | II |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | I |  |  |  | II |  |  |  | III |  |  |  | IV |  |  |  |
|  | 1 | 6.6 | 6.3 | 6.5 | 6.4 | 6.6 | 6.7 | 6.6 | 6.6 | 6.7 | 7.0 | 7.6 | 7.3 | 7.0 | 6.6 | 6.8 | 6.6 |
|  | 2 | 6.7 | 6.4 | 6.5 | 6.4 | 6.5 | 6.7 | 6.5 | 6.5 | 6.8 | 7.3 | 7.8 | 7.3 | 6.9 | 6.7 | 6.8 | 6.5 |
|  | 3 | 6.8 | 6.3 | 6.1 | 6.3 | 6.4 | 6.5 | 6.5 | 6.8 | 7.1 | 7.3 | 7.5 | 7.2 | 6.9 | ． 7 | 6.6 | 6.6 |
| I | 4 | 6.7 | 6.2 | 6.0 | 6.2 | 6.2 | 6.5 | 6.6 | 6.9 | 7.2 | 7.4 | 7.4 | 7.2 | 6.8 | 6.5 | 6.7 | 6.8 |
|  | 5 | 6.8 | 6.3 | 6. |  | 6.2 | crack |  | 6.9 | 7.1 | 7.3 | 7.5 | 7.0 | 6.9 | 6.8 | ． 0 | ． 1 |
|  | 6 | 6.7 | 6.2 |  |  | 6.4 |  |  | 7.0 | 7.2 | 7.3 | 7.0 | 7.1 | 7.1 | 7.1 | 6.8 |
|  | 7 | 6.6 | 6.3 | 5.9 | 6.1 | 6 | 6.5 | 6.5 |  | 6.6 | 6.9 | 7.2 | 7.3 | 7.1 | 7.3 | 7.1 | 7.1 | 6.8 |
|  | 8 | 6.5 | 6.2 | 5.9 |  | 6.8 | 6.6 | 6.4 | 6.6 | 6.8 | 7.1 | 7.3 | 7.2 | 7.1 | 7.0 | 6.9 | 6.8 |
|  | 9 | 6.6 | 6.5 | 6.3 | 6.4 | 6.7 | 6.3 | 6.3 | 6.9 | 96.6 | 7.1 | 7.4 | 7.1 | 7.1 | 6.9 | 6.8 | 7 |
|  | 10 | 6.7 | 6.6 | 6.4 | 6.3 | 6.5 | 6.4 | 6.4 | 7.0 | 6.8 | 7.3 | 7.2 | 6.9 | 6.8 | 6.8 | 6.8 | 6.8 |
|  | 11 | 6.6 | 6.5 | 6.3 | 6.3 | 6.6 | 6.4 | 6.3 | 6.8 | 7.0 | 7.5 | 7.2 | 6.8 | 6.8 | 6.9 | 6.9 | 6.7 |
| II | 12 | 6.5 | 6.3 | 6.3 | 6.2 | 6.5 | 6.4 | 6.8 | 6.8 | 7.1 | 7.4 | 7.1 | 6.9 | 6.7 | 6.7 | 6.9 | 6.8 |
|  | 13 | 6.3 | 6.2 |  | 6.0 | 6.1 | 6.4 | 6.8 | 7.0 | 7.2 | 7.3 | 7.0 | 6.8 | 6.7 | 6.9 | 7.2 | 6.9 |
|  | 14 | 6.2 | 6.3 | 6.1 | 6.1 | 6.3 | 6.5 | 6.7 | 6.9 | 7.2 | 7.2 | 7.1 | 6.9 | 6.9 | 7.2 | 4 | 6.8 |
|  | 15 | 6.3 | 6.0 | 6.1 | 6.3 | 6.4 | 6.3 | 6.6 | 6.8 | 7.1 | 7.2 | 7.1 | 7.0 | 7.2 | 7.2 | 2 | 6.7 |
|  | 16 | 6.2 | 6.0 | 6.3 | 6.7 | 6.5 | 6.2 | 6.5 | 6.7 | 7.0 | 7.2 | 7.2 | 7.2 | 7.2 | 7.3 | 7.1 | 6.7 |
|  | 17 | 6.3 | 6.2 | 6.6 | 6.6 | 6.4 | 6.2 | 6.5 | 6.8 | 7.0 | 7.1 | 7.1 | 7.1 | 7.0 | 7.2 | 7.0 | 6.5 |
|  | 18 | 6.7 | 6.6 | 6.5 | 6.4 | 6.1 | 6.2 | 6.3 | 6.6 | 6.9 | 7.1 | 7.0 | 7.1 | 6.8 | 6.9 | 6.9 | 6.7 |
| III | 19 | 6.8 | 6.6 | 6.6 | 6.5 | 6.2 | 6.3 | 6.2 | 6.7 | 7.2 | 7.1 | 6.9 | 6.9 | 6.9 | 7.0 | 6.9 | 6.8 |
|  | 20 | 6.8 | 6.6 | 6.5 | 6.3 | 6.1 | 6.2 | 6.4 | 7.2 | 7.3 | 7.1 | 6.8 | 6.8 | 6.9 | 6.9 | 6.9 | 6.7 |
|  | 21 | 6.5 | 6.4 | 6.4 | 6.4 | 6.3 | 6.4 | 6.7 | 7.1 | 7.3 | 7.0 | 6.8 | 6.7 | 6.9 | 7.0 | 6.9 | 6.6 |
|  | 22 | 6.5 | 6.4 | 6.4 | 6.3 | 6.3 | 6.5 | 6.8 | $7.1$ | $7.1$ | 7.0 | 6.9 | 6.8 | 7.0 | 7.3 | 6.8 | 6.5 |


| 自 | 帚 | 㮰 | $n$ | dav <br> $\%$ |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| 63 | 6.74 | 7.6 | 0.33 | 0.3 |
| 6.4 | 6.77 | 7.8 | 0.39 | 0.6 |
| 6.1 | 6.73 | 7.5 | 0.39 | 0.0 |
| 6 | 6.71 | 7.4 | 0.44 | －0．3 |
| 6 | 6.76 | 7.5 | 0.44 | 0.4 |
| 6 | 6.74 | 73 | 0.41 | 0.2 |
| 5.9 | 6.74 | 73 | 0.43 | 0.3 |
| 59 | 6.72 | 73 | 0.39 | －0．1 |
| 63 | 6.73 | 7.4 | 0.33 | 0.1 |
| 63 | 6.73 | 73 | 0.29 | 0.1 |
| 63 | 6.73 | 75 | 0.34 | 0.0 |
| 6.2 | 6.71 | 7.4 | 0.33 | －0．2 |
| 6 | 6.69 | 73 | 0.43 | －0．6 |
| 6.1 | 6.74 | 7.4 | 0.43 | 0.2 |
| 6 | 6.72 | 7.2 | 0.44 | －0．1 |
| 6 | 6.75 | 73 | 0.43 | 0.4 |
| 6.2 | 6.73 | 7.2 | 0.35 | 0.0 |
| 6.1 | 6.68 | 7.1 | 0.31 | －0．8 |
| 6.2 | 6.73 | 7.2 | 0.30 | 0.0 |
| 6.1 | 6.72 | 73 | 0.35 | －0．1 |
| 63 | 6.71 | 73 | 0.30 | －0．2 |
| 63 | 6.73 | 73 | 0.32 | 0.1 |


| $\min$ | 6.2 | 6 | 5.9 | 6 | 6.1 | 6.2 | 6.2 | 6.5 | 6.6 | 7 | 6.8 | 6.7 | 6.7 | 6.5 | 6.6 | 6.5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| aver | 6.56 | 6.34 | 6.27 | 6.30 | 6.40 | 6.42 | 6.52 | 6.82 | 7.02 | 7.20 | 7.20 | 7.01 | 6.95 | 6.94 | 6.94 | 6.72 |
| $\max$ | 6.8 | 6.6 | 6.6 | 6.7 | 6.8 | 6.7 | 6.8 | 7.2 | 7.3 | 7.5 | 7.8 | 7.3 | 7.3 | 7.3 | 7.4 | 7.1 |
| $\mathbf{S}$ | 0.20 | 0.18 | 0.23 | 0.17 | 0.20 | 0.15 | 0.17 | 0.19 | 0.19 | 0.14 | 0.26 | 0.18 | 0.16 | 0.22 | 0.18 | 0.14 |


| thickness， mm | $\min$ | aver | $\max$ | S | n |
| :--- | :---: | :---: | :---: | :---: | :---: |
| The cylindrical part | 5.9 | 6.73 | 7.8 | 0.36 | 352 |


thickness，mm

conditional min－．－．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．conditional max | scale | 4.7 | 5.09 | 5.28 | 5.48 | 5.67 | 5.86 | 6.06 | 6.25 | 6.44 | 6.64 | 6.83 | 7.03 | 7.22 | 7.41 | 7.61 | 7.8 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

sample
I1

Fig．4．Map of the wall thickness of the specimen I1 in original state．
On the right of the map the deviation of the mean cross－sectional thickness from the average thickness of the cylinder（dav）is specified．The figure indicates the location of the crack formed after the destruction of the specimen；min，aver，max－the minimum，average and maximum values， respectively； S －standard deviation； n －number of measurements．

Table 5. The wall thickness of the specimen I1 in original state, mm .

| Section <br> $\#$ | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ | $\mathbf{9}$ | $\mathbf{1 0}$ | $\mathbf{1 1}$ | $\mathbf{1 2}$ | $\mathbf{1 3}$ | $\mathbf{1 4}$ | $\mathbf{1 5}$ | $\mathbf{1 6}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 6.6 | 6.3 | 6.5 | 6.4 | 6.6 | 6.7 | 6.6 | 6.6 | 6.7 | 7.0 | 7.6 | 7.3 | 7.0 | 6.6 | 6.8 | 6.6 |
| 2 | 6.7 | 6.4 | 6.5 | 6.4 | 6.5 | 6.7 | 6.5 | 6.5 | 6.8 | 7.3 | 7.8 | 7.3 | 6.9 | 6.7 | 6.8 | 6.5 |
| 3 | 6.8 | 6.3 | 6.1 | 6.3 | 6.4 | 6.5 | 6.5 | 6.8 | 7.1 | 7.3 | 7.5 | 7.2 | 6.9 | 6.7 | 6.6 | 6.6 |
| $\mathbf{4}$ | $\mathbf{6 . 7}$ | $\mathbf{6 . 2}$ | $\mathbf{6 . 0}$ | $\mathbf{6 . 2}$ | $\mathbf{6 . 2}$ | $\mathbf{6 . 5}$ | $\mathbf{6 . 6}$ | $\mathbf{6 . 9}$ | $\mathbf{7 . 2}$ | $\mathbf{7 . 4}$ | $\mathbf{7 . 4}$ | $\mathbf{7 . 2}$ | $\mathbf{6 . 8}$ | $\mathbf{6 . 5}$ | $\mathbf{6 . 7}$ | $\mathbf{6 . 8}$ |
| 5 | 6.8 | 6.3 | 6.0 | 6.1 | 6.2 | 6.5 | 6.6 | 6.9 | 7.1 | 7.3 | 7.5 | 7.0 | 6.9 | 6.8 | 7.0 | 7.1 |
| 6 | 6.7 | 6.2 | 6.0 | 6.1 | 6.4 | 6.6 | 6.5 | 6.7 | 7.0 | 7.2 | 7.3 | 7.0 | 7.1 | 7.1 | 7.1 | 6.8 |
| 7 | 6.6 | 6.3 | $\mathbf{5 . 9}$ | 6.1 | 6.6 | 6.5 | 6.5 | 6.6 | 6.9 | 7.2 | 7.3 | 7.1 | 7.3 | 7.1 | 7.1 | 6.8 |
| 8 | 6.5 | 6.2 | $\mathbf{5 . 9}$ | 6.3 | 6.8 | 6.6 | 6.4 | 6.6 | 6.8 | 7.1 | 7.3 | 7.2 | 7.1 | 7.0 | 6.9 | 6.8 |
| 9 | 6.6 | 6.5 | 6.3 | 6.4 | 6.7 | 6.3 | 6.3 | 6.9 | 6.6 | 7.1 | 7.4 | 7.1 | 7.1 | 6.9 | 6.8 | 6.7 |
| 10 | 6.7 | 6.6 | 6.4 | 6.3 | 6.5 | 6.4 | 6.4 | 7.0 | 6.8 | 7.3 | 7.2 | 6.9 | 6.8 | 6.8 | 6.8 | 6.8 |
| 11 | 6.6 | 6.5 | 6.3 | 6.3 | 6.6 | 6.4 | 6.3 | 6.8 | 7.0 | 7.5 | 7.2 | 6.8 | 6.8 | 6.9 | 6.9 | 6.7 |
| $\mathbf{1 2}$ | $\mathbf{6 . 5}$ | $\mathbf{6 . 3}$ | $\mathbf{6 . 3}$ | $\mathbf{6 . 2}$ | $\mathbf{6 . 5}$ | $\mathbf{6 . 4}$ | $\mathbf{6 . 8}$ | $\mathbf{6 . 8}$ | $\mathbf{7 . 1}$ | 7.4 | $\mathbf{7 . 1}$ | $\mathbf{6 . 9}$ | $\mathbf{6 . 7}$ | $\mathbf{6 . 7}$ | $\mathbf{6 . 9}$ | $\mathbf{6 . 8}$ |
| 13 | 6.3 | 6.2 | 6.2 | 6.0 | 6.1 | 6.4 | 6.8 | 7.0 | 7.2 | 7.3 | 7.0 | 6.8 | 6.7 | 6.9 | 7.2 | 6.9 |
| 14 | 6.2 | 6.3 | 6.1 | 6.1 | 6.3 | 6.5 | 6.7 | 6.9 | 7.2 | 7.2 | 7.1 | 6.9 | 6.9 | 7.2 | 7.4 | 6.8 |
| 15 | 6.3 | $\mathbf{6 . 0}$ | 6.1 | 6.3 | 6.4 | 6.3 | 6.6 | 6.8 | 7.1 | 7.2 | 7.1 | 7.0 | 7.2 | 7.2 | 7.2 | 6.7 |
| 16 | 6.2 | $\mathbf{6 . 0}$ | 6.3 | 6.7 | 6.5 | 6.2 | 6.5 | 6.7 | 7.0 | 7.2 | 7.2 | 7.2 | 7.2 | 7.3 | 7.1 | 6.7 |
| 17 | 6.3 | 6.2 | 6.6 | 6.6 | 6.4 | 6.2 | 6.5 | 6.8 | 7.0 | 7.1 | 7.1 | 7.1 | 7.0 | 7.2 | 7.0 | 6.5 |
| 18 | 6.7 | 6.6 | 6.5 | 6.4 | 6.1 | 6.2 | 6.3 | 6.6 | 6.9 | 7.1 | 7.0 | 7.1 | 6.8 | 6.9 | 6.9 | 6.7 |
| $\mathbf{1 9}$ | $\mathbf{6 . 8}$ | $\mathbf{6 . 6}$ | $\mathbf{6 . 6}$ | $\mathbf{6 . 5}$ | $\mathbf{6 . 2}$ | $\mathbf{6 . 3}$ | $\mathbf{6 . 2}$ | $\mathbf{6 . 7}$ | $\mathbf{7 . 2}$ | $\mathbf{7 . 1}$ | $\mathbf{6 . 9}$ | $\mathbf{6 . 9}$ | $\mathbf{6 . 9}$ | $\mathbf{7 . 0}$ | $\mathbf{6 . 9}$ | $\mathbf{6 . 8}$ |
| 20 | 6.8 | 6.6 | 6.5 | 6.3 | 6.1 | 6.2 | 6.4 | 7.2 | 7.3 | 7.1 | 6.8 | 6.8 | 6.9 | 6.9 | 6.9 | 6.7 |
| 21 | 6.5 | 6.4 | 6.4 | 6.4 | 6.3 | 6.4 | 6.7 | 7.1 | 7.3 | 7.0 | 6.8 | 6.7 | 6.9 | 7.0 | 6.9 | 6.6 |
| 22 | 6.5 | 6.4 | 6.4 | 6.3 | 6.3 | 6.5 | 6.8 | 7.1 | 7.1 | 7.0 | 6.9 | 6.8 | 7.0 | 7.3 | 6.8 | 6.5 |

Table 6. The wall thickness in the sections I, II, III, of I1 specimen in original state, mm .

| Section | \# of the point number in cross-section |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | average |
| I | 6.7 | 6.2 | 6.0 | 6.2 | 6.2 | 6.5 | 6.6 | 6.9 | 7.2 | 7.4 | 7.4 | 7.2 | 6.8 | 6.5 | 6.7 | 6.8 | 6.71 |
| II | 6.5 | 6.3 | 6.3 | 6.2 | 6.5 | 6.4 | 6.8 | 6.8 | 7.1 | 7.4 | 7.1 | 6.9 | 6.7 | 6.7 | 6.9 | 6.8 | 6.71 |
| III | 6.8 | 6.6 | 6.6 | 6.5 | 6.2 | 6.3 | 6.2 | 6.7 | 7.2 | 7.1 | 6.9 | 6.9 | 6.9 | 7.0 | 6.9 | 6.8 | 6.73 |
| average |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 6.71 |



| 直 | 产 | 皆 | a |  |
| :---: | :---: | :---: | :---: | :---: |
| 6.2 | 6.73 | 7.5 | 0.37 | 4.5 |
| 5.9 | 6.54 | 7.6 | 0.48 | 1.6 |
| 5.6 | 6.44 | 7.4 | 0.53 | 0.1 |
| 5.2 | 6.36 | 7.2 | 0.58 | －1．3 |
| 5 | 637 | 7.3 | 0.61 | －1．1 |
| 5 | 634 | 7.2 | 0.64 | －1．5 |
| 4.7 | 631 | 7.2 | 0.73 | －1．9 |
| 4.7 | 6.29 | 7.2 | 0.67 | －2．2 |
| 53 | 6.29 | 7.2 | 0.53 | －2．3 |
| 5.4 | 6.31 | 7.2 | 0.49 | －2．0 |
| 5.4 | 637 | 7.4 | 0.55 | －1．1 |
| 5.5 | 6.38 | 73 | 0.51 | －0．9 |
| 5.4 | 633 | 7.2 | 0.63 | －1．7 |
| 5.4 | 6.38 | 7.2 | 0.62 | －1．0 |
| 5.3 | 638 | 7.2 | 0.64 | －1．0 |
| 5.3 | 638 | 7.2 | 0.61 | －1．0 |
| 5.6 | 6.47 | 7.2 | 0.50 | 0.5 |
| 5.7 | 6.44 | 7.1 | 0.40 | 0.0 |
| 5.7 | 6.46 | 7.1 | 0.41 | 0.4 |
| 5.9 | 6.53 | 7.2 | 0.41 | 1.5 |
| 6.1 | 6.64 | 7.2 | 0.36 | 3.1 |
| 65 | 6.91 | 7.5 | 0.35 | 7.4 |



| thickness， mm | $\min$ | aver | $\max$ | S | n |
| :--- | :---: | :---: | :---: | :---: | :---: |
| The cylindrical part | 4.7 | 6.44 | 7.6 | 0.54 | 352 |


thickness，mm
sample
I1

Fig．5．Map of the wall thickness after specimen destruction and places of tensile samples $30 \mathrm{~mm} \times$ 180 mm cutting． $\mathrm{K}, \mathrm{O}$－samples in circumferential and axial direction，respectively；low index－ value of residual deformation in the hoop direction after failure．All other symbols－are the same as in Fig． 4.

Table 7．The wall thickness in the sections I，II，III，I1 after specimen fracture，mm．

| Section | \＃point number in the cross－section |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | average |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |  |
| I | 6.4 | 5.7 | 5.2 | 5.6 | 5.9 | 6.0 | 6.3 | 6.7 | 7.0 | 7.2 | 7.2 | 7.0 | 6.5 | 6.2 | 6.3 | 6.5 | 6.36 |
| II | 5.9 | 5.8 | 5.5 | 5.7 | 6.1 | 6.0 | 6.4 | 6.7 | 7.0 | 7.3 | 7.0 | 6.7 | 6.5 | 6.3 | 6.6 | 6.6 | 6.38 |
| III | 6.5 | 6.2 | 6.2 | 6.2 | 5.7 | 5.8 | 6.0 | 6.5 | 7.0 | 7.1 | 6.7 | 6.8 | 6.7 | 6.7 | 6.8 | 6.5 | 6.46 |
| average |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 6.40 |

Note：The wall thickness in the places of fracture was measured with a caliper：4．5－4．8 mm．

Loading of the specimen by internal pressure was done stepwise (Fig. 6), after each step the pressure was released to 0 . Steps $1 \ldots 20$ were held in the water jacket, and steps $21 . .25$ out of it. Loading in steps $1 \ldots 20$ was made by holding max pressure during 0.5 ... 3 min . For reducing pressure fluctuations 2 additional high pressure receivers were included in the hydraulic system.


Fig. 6. Steps of internal pressure loading of the specimen I1. $P_{w}, P_{h}$ - working pressure and test pressure; $P_{y}$ - yield pressure; $P_{b}, P_{b}^{*}$ - the maximum pressure that sustained the specimen and the pressure at which the failure occurred; 2 receivers - the pressure in the two paired receivers connected without the specimen.

According to test results of the sample I1:
$\mathrm{P}_{\mathrm{y}}=20 \mathrm{MPa}, \mathrm{P}_{\mathrm{b}}=27.59 \mathrm{MPa}, \mathrm{P}_{\mathrm{b}}{ }^{*}=27.44 \mathrm{MPa}$.
Judging by the nature of crack and loading diagram (Fig.6), fracture of specimen I1 had ductile character.

Table 8. Change in the volume of specimen I1 during test in the water jacket, (WJ). Steps 1 ... 20.


Note: $\Delta \mathrm{V}_{\mathrm{ti}}$ - the maximum (full) change of volume at each step was determined at the end of exposure to max pressure; $\Delta \mathrm{V}_{\mathrm{pi}}$ - residual change of volume at the appropriate step after pressure release. Changing the volume was determined by burettes of water jacket (Fig.7) as the difference between levels of the liquid columns multiplied by a calibration coefficient and with the addition of $7.4 \%$ taking into account the error of the burette A , and $1.78 \%$ for burettes B.

Table 9. Perimeters ( Pp mm ) of the specimen I1 and change of its weight (with water) after steps 20... 25 (out of the water jacket).

| Step \# | $\begin{aligned} & \mathrm{P}_{\max } \\ & \mathrm{MPa} \\ & \hline \end{aligned}$ | Perimeter designation | Section \# |  |  | average | The change in weight, kg |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1 | II | III |  |  |
| 0 | 0 | $\mathrm{Po}=\mathrm{P}_{\mathrm{H}}$ | 693.5 | 693.5 | 693.5 | 693.5 |  |
| 20 | 23.87 | $\mathrm{P}_{20}$ | 708.0 | 708.2 | 707.8 | 708 | 1.475 |
| 21 | 24.62 | $\mathrm{P}_{21}$ | 711.2 | 711.3 | 710.4 | 710.97 | 1.658 |
| 22 | 25.71 | $\mathrm{P}_{22}$ | 717 | 717.6 | 716.2 | 716.93 | 2.225 |
| 23 | 26.6 | $\mathrm{P}_{23}$ | 725.4 | 726.1 | 723.3 | 724.93 | 3.100 |
| 24 | 27.41 | $\mathrm{P}_{24}$ | 738.6 | 743.1 | 734.4 | 738.7 | 4.525 |
| 25 | 27.59 | $\mathrm{P}_{25}=\mathrm{P}_{\mathrm{K}}$ | 744 | 753 | 741 | 746 | - |

Results of perimeter changing are given at Fig. 8 (in accordance with Table 9).


Fig.8. Perimeter (Pp) of specimen I1 measured in sections I, II, III after steps 20-25.
Table 10. Perimeter ( $\mathrm{P}_{\mathrm{K}}$ ) after specimen destruction.

| Section \# * |  | $\mathrm{P}_{\mathrm{K}}, \mathrm{mm}$. |
| :---: | :---: | :---: |
|  | 1 | 699.6 |
|  | 2 | 719.5 |
|  | 3 | 732.4 |
| Sec. I | 4 | 742.5 |
|  | 5 | 749.5 |
|  | 6 | - |
|  | 7 | - |
|  | 8 | - |
|  | 9 | - |
|  | 10 | - |
|  | 11 | - |
| Sec. II | 12 | - |
|  | 13 | 753.8 |
|  | 14 | 753 |
|  | 15 | 751.2 |
|  | 16 | 748.8 |
|  | 17 | 745.6 |
|  | 18 | 741.4 |
| Sec. III | 19 | 737.8 |
|  | 20 | 730.5 |
|  | 21 | 720 |
|  | 22 | 702 |



Fig. 9. Specimen I1. a - after step 24; b - after failure (step 25).

*     - Perimeter was determined in the sections of wall thickness measurements (Fig.1a).


Fig.10. Sample for tensile test cut out the specimen I1 after its destruction.

## Protocol of specimen I2 (with defect).

For the manufacture of the specimen was used piece of pipe \#7, weight 32.7 kgf (Fig.12).
Table 11. Axial dimensions of the specimen I1 in the original state.

| $\#$ | Linear size, mm | Sector |  |  |  | IV |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
|  | I | II | III | IV | average |  |
| 1 | length of the pipe piece, $1_{\mathrm{o}}$ | 948 | 948 | 946 | 947 | 947.25 |
| 2 | length between the inner surfaces of the plates <br> (bottoms) after welding | 954 | 954 | 952 | 953 | 953.25 |

Note: The measurements were made in the middle of the sectors I ... IV, (Fig.1).
Table 12. Specimen I1 perimeter before $\left(\mathrm{P}_{\mathrm{H}}\right)$ and after destruction $\left(\mathrm{P}_{\mathrm{K}}\right)$.

| The cross section $\rightarrow$ | $\mathrm{I}^{*}$ | $\mathrm{II}^{*}$ | average |
| :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\mathrm{H}}, \mathrm{mm}$ | 692.3 | 692.3 | 692.3 |
| $\mathrm{P}_{\mathrm{K}}, \mathrm{mm}$ | 692.3 | 692.3 | 692.3 |

Table 13. Wall thickness of the specimen in original state, mm.

| Section \# | Point \# |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | average |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |  |
| I* | 7.1 | 6.7 | 6.6 | 6.6 | 6.8 | 6.6 | 6.4 | 6.4 | 6.5 | 6.8 | 6.8 | 6.8 | 6.6 | 7.0 | 7.1 | 7.3 | 6.76 |
| II* | 6.8 | 6.5 | 6.5 | 6.9 | 6.6 | 6.1 | 6.1 | 6.2 | 6.9 | 6.9 | 7.2 | 7.2 | 7.1 | 6.9 | 7.3 | 6.9 | 6.76 |
| average |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 6.76 |

Note: After the destruction of the specimen the thickness of the wall in sections I* and II* has not changed.

Weight of welded specimen: 60.7 kg . Weight of the specimen with water: 92.6 kg . Water temperature: $12.5^{\circ} \mathrm{C}$. Water weight: 31.9 kg . Internal volume of the specimen 31.9 liters. Weight of specimen filled with water and hydraulic armature: 93.3 kg . The initial linear dimensions of the defect: $133 \times 102 \mathrm{~mm}$. Length of $\operatorname{arc} \mathrm{A}$ (Fig,11): $\mathrm{A}=586 \mathrm{~mm}$.


Fig. 11. Arc A.


Fig.12. Specimen I2: a - before the test, b - pipe edge prepared for welding; $\mathrm{c}, \mathrm{d}$ - welding of the lower bottom; e - top end of the specimen; f - defect (numbers near the points indicate the wall thickness).

Loading of the specimen by internal pressure was done stepwise (Fig.13), after each step the pressure was released to 0 . Loading in steps $1 \ldots .20$ was made by holding max pressure during the time necessary for reading of strain gauges mounted on the specimen surface (Fig.14).


Fig.13. Loading of the specimens I2 and I1 by internal pressure: a - loading steps of the specimen with defect (I2); b-I1 and I2 loading; c- before the last and last steps (enlarged). Designations as in Fig. 6.

Table 14.Experimental strains (gauges 1..8, Fig.14).

| Step \# | P, MPa | Defect |  | Defect |  | Pipe |  | Pipe |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | axial strain |  | hoop strain |  | axial strain |  | hoop strain |  |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| 1 | 1.45 | $7.79 \mathrm{E}-05$ | $7.34 \mathrm{E}-05$ | 0.00033 | 0.00033 | $2.29 \mathrm{E}-05$ | $2.29 \mathrm{E}-05$ | 0.00011 | 0.00011 |  |
| 2 | 2.45 | $9.17 \mathrm{E}-05$ | 0.000115 | 0.000532 | 0.000536 | $3.21 \mathrm{E}-05$ | $3.67 \mathrm{E}-05$ | 0.000193 | 0.000188 |  |
| 3 | 3.34 | 0.000128 | 0.000147 | 0.000724 | 0.000734 | $5.5 \mathrm{E}-05$ | $4.58 \mathrm{E}-05$ | 0.000257 | 0.000266 |  |
| 4 | 4.32 | 0.000174 | 0.000193 | 0.000935 | 0.000935 | $6.42 \mathrm{E}-05$ | $6.42 \mathrm{E}-05$ | 0.00033 | 0.000339 |  |
| 5 | 5.04 | 0.000193 | 0.000211 | 0.001119 | 0.001119 | $7.34 \mathrm{E}-05$ | $6.42 \mathrm{E}-05$ | 0.00039 | 0.000385 |  |
| 6 | 5.83 | 0.000229 | 0.000284 | 0.001394 | 0.001366 | $8.25 \mathrm{E}-05$ | $8.25 \mathrm{E}-05$ | 0.000449 | 0.000445 |  |
| 7 | 6.9 | 0.000541 | 0.000633 | 0.001907 | 0.001816 | 0.000101 | 0.000101 | 0.000523 | 0.000523 |  |
| 8 | 8.12 | 0.000779 | 0.001522 |  |  | 0.000133 | 0.000128 | 0.000601 | 0.000605 |  |
| 9 | 9.64 |  |  |  |  | 0.00017 | 0.000174 | 0.000697 | 0.000692 |  |



Fig. 14. Measurement of specimen I2 strains: a - gauges 5, 6, 7, 8 location; b-gauges 1, 2, 3, 4 location; c - ISD-3 measuring device, $\mathrm{d}, \mathrm{e}-$ specimen during the test.

Length measuring the of bases K and O in circumferential and axial direction, correspondingly, was done after steps $9 \ldots 12$ (Table.15). Measurement was carried out by a ruler.

After the step \#10 maximal residual deflection in the defect had reached a depth of the defect (Fig.15).

Table 15. Base lengths in the defect and specimen weight

|  |  | Linear dimension, mm |  |  | Arc A <br> Step \# | P, MPa |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | K | O | (length x width) <br> of the defect | Weight of <br> mm |  |  |
| 9 | 9.64 | 44.8 | 44.6 | $133 \times 102$ | 586 | 93.3 |
| 10 | 11.78 | 45.9 | 44.6 |  |  | - |
| 11 | 13.49 | 47.2 | 44.6 | $133 \times 107.2$ | 586 | 93.3 |
| 12 (last) | 13.83 | 47.2 | 44.6 | $133 \times 110$ | 586 | - |



Fig.15. Defect after step \#10.


Fig.16. Defect after step \#11.

Some general views of specimen after destruction are given at Fig. 17...19.


Fig.17. Destruction of the specimen: a - general view; $\mathrm{b}, \mathrm{c}-$ the destruction in the defect.


Fig.18. Defect wall thickness before (a) and after (b) destruction. (Dimensions in millimeters).
At Fig. 18b also is given the thickness at the contour of the destruction measured with a caliper.


Fig. 19. Fracture in defect zone.

## Protocol of specimen I3 (with defect and bandage).

Loading of the specimen by internal pressure was done stepwise, after each step the pressure was released to 0 .

The chronology of measurements and loading of the sample by internal pressure is given below:

- stage 1 ... 5 - measurement of strain using strain gauges installed in the defect and regular part of the pipe, before the start of plastic deformation in the defect (without bandage).
- installation of thebandage.
- stage $1 \ldots 13$ - measurement of strain using strain gauges installed in the defect, regular part of the tube and on the surface of the bandage.
- stage 14 ... 18 - measurement of the perimeter of the pipe reinforced by bandage, determination of changes in specimen weight.

For the manufacture of the sample was pipe section \#6 (Fig. 22a). Weight of the pipe section ith defect -32.7 kgf .

Table 16. The length of the cylindrical portion of the sample I3 and axial dimensions in the original condition and after the destruction.

| $\#$ | Linear size, mm | Sector |  |  |  | IV |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
|  |  | II | III | IVerage |  |  |
| 1 | length of the pipe section, $\mathrm{l}_{\mathrm{o}}$ | 947 | 946 | 946 | 947 | 946.5 |
| 2 | length between inner surfaces of the sealing <br> bottoms before test | 954 | 955 | 953 | 956 | 954.5 |
| 3 | length between inner surfaces of the sealing <br> bottoms before test | 954 | 955 | 953 | 956 | 954.5 |

Note: The measurements were done in the middle of the sectors I ... IV, (Fig. 1).
Table 17. The perimeter of the I3 sample in its original state, during the test, and after destruction mm .

| Sec. $\rightarrow$ | 4 | 5 | 6 | 8 | $9\left(I^{*}\right)$ | $9\left(I^{*}\right)$ | 9,5 | 10 | 11,5 | 13 | $14\left(I^{*}\right)$ | 18 | 19 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase $\downarrow$ |  |  |  |  | Transition |  |  |  |  |  |  |  |  |
| 0 | 693.5 | 693.5 | 693.5 | 693.5 | 693.5 |  |  |  |  |  | 693.5 | 693.0 | 693.0 |
| 0 |  |  |  |  |  | $\mathbf{7 3 1 . 6}$ | $\mathbf{7 3 2 . 6}$ | $\mathbf{7 3 5 . 8}$ | $\mathbf{7 3 7 . 5}$ | $\mathbf{7 3 6 . 5}$ | $\mathbf{7 3 5 . 0}$ |  |  |
|  |  |  |  |  |  |  |  |  | W | W | W |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 13 | 698.8 | 698.7 | 698.8 | 697.2 | 695.2 | $\mathbf{7 3 1 . 6}$ | $\mathbf{7 3 3 . 2}$ | $\mathbf{7 3 6 . 0}$ | $\mathbf{7 3 8 . 8}$ | $\mathbf{7 3 7 . 8}$ | $\mathbf{7 3 5 . 0}$ | 699.8 | 699.4 |
| 14 | 703.2 | 703.0 | 703.8 | 700.4 | 697.0 | $\mathbf{7 3 2 . 4}$ | $\mathbf{7 3 3 . 6}$ | $\mathbf{7 3 6 . 8}$ | $\mathbf{7 3 8 . 8}$ | $\mathbf{7 3 7 . 6}$ | $\mathbf{7 3 5 . 5}$ | 704.2 | 704.2 |
| 15 | 711.0 | 710.6 | 710.8 | 705.2 | 700.0 | $\mathbf{7 3 3 . 5}$ | $\mathbf{7 3 4 . 5}$ | $\mathbf{7 3 7 . 0}$ | $\mathbf{7 3 9 . 0}$ | $\mathbf{7 3 7 . 6}$ | $\mathbf{7 3 5 . 5}$ | 714.2 | 714.0 |
| 16 | 723.2 | 723.0 | 722.0 | 711.0 | 702.8 | $\mathbf{7 3 4 . 6}$ | $\mathbf{7 3 4 . 8}$ | $\mathbf{7 3 7 . 0}$ | $\mathbf{7 3 9 . 0}$ | $\mathbf{7 3 7 . 8}$ | $\mathbf{7 3 5 . 5}$ | 726.8 | 726.0 |
| 17 | 738.2 | 739.6 | 737.0 | 717.2 | 705.8 | $\mathbf{7 3 5 . 8}$ | $\mathbf{7 3 5 . 2}$ | $\mathbf{7 3 7 . 0}$ | $\mathbf{7 3 9 . 4}$ | $\mathbf{7 3 7 . 8}$ | $\mathbf{7 3 6 . 0}$ | 743.0 | 741.8 |
| 18 | 761.2 | 764.0 | 760.0 | 729.0 | 709.2 | $\mathbf{7 3 6 . 2}$ | $\mathbf{7 3 5 . 2}$ | $\mathbf{7 3 7 . 0}$ | $\mathbf{7 3 9 . 4}$ | $\mathbf{7 3 7 . 8}$ | $\mathbf{7 3 6 . 0}$ | $\underline{764.0}$ | $\underline{764.0}$ |
| $18^{* *}$ |  |  |  |  | 699.0 |  |  | 695.0 |  | 694.8 | 695.0 |  |  |

Notes: After installation of the bandage the perimeter of the pipe at areas not covered with bandage has not changed. W - wire strain gauges on a bandage. Bold values relate to the bandage. Underlining values relate to measurements at the area of destruction. The sample is divided into 22 conditional sections (see. Fig. 1). Cross-section 9.5 is located between the 9th and 10th sections. Transition - the area of the beginning of the bandage (see. Fig. 24).

*     - one value for the pipe other for the bandage.
** - After removal of the bandage.

In the middle of the defect in the ring（ R ）and axial（A）directions were punched measuring bases（see．Figure 22b）： $\mathrm{R}=44.8 \mathrm{~mm}, \mathrm{~A}=45.0 \mathrm{~mm}$ ．After the destruction of the sample and removal of the bandage： $\mathrm{R}=45.4 \mathrm{~mm}, \mathrm{~A}=45.0 \mathrm{~mm}$ ．The measurement was made by the metal ruler．The length and width of the defect in the initial state，measured in the middle by caliper： $133.2 \times 102.2 \mathrm{~mm}$ ．After the destruction of the sample and removal of the bandage length and width amounted： $133.3 \times 103.2 \mathrm{~mm}$ ．


| 白 | 岛 | 皆 | $n$ | $\begin{gathered} \text { dav } \\ \% \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| 6.6 | 6.94 | 7.4 | 0.25 | 0.7 |
| 6.5 | 6.97 | 7.4 | 0.29 | 1.2 |
| 6.4 | 6.88 | 7.6 | 0.33 | －0．2 |
| 6.4 | 6.95 | 7.6 | 0.30 | 0.9 |
| 6.1 | 691 | 7.4 | 0.35 | 0.3 |
| 6.1 | 6.83 | 7.4 | 0.36 | －0．9 |
| 6.6 | 6.93 | 7.3 | 0.24 | 0.6 |
| 6.3 | 6.86 | 7.2 | 0.24 | －0．5 |
| 6.2 | 6.86 | 7.5 | 0.35 | －0．5 |
| 6.4 | 6.91 | 7.5 | 0.30 | 0.3 |
| 6.5 | 6.99 | 7.4 | 0.23 | 1.5 |
| 6.5 | 6.84 | 7.5 | 0.28 | －0．8 |
| 6.3 | 6.91 | 7.5 | 0.36 | 0.4 |
| 63 | 6.91 | 7.5 | 0.37 | 0.3 |
| 6.2 | 6.85 | 7.4 | 0.34 | －0．6 |
| 6.2 | 6.83 | 7.3 | 0.34 | －0．8 |
| 6.1 | 6.83 | 7.2 | 0.33 | －0．8 |
| 6.1 | 6.82 | 7.1 | 0.33 | －1．0 |
| 6.4 | 6.81 | 7.3 | 0.30 | －1．1 |
| 6.5 | 6.86 | 7.4 | 0.27 | －0．5 |
| 6.4 | 6.91 | 7.5 | 0.33 | 0.3 |
| 6.7 | 6.98 | 7.6 | 0.29 | 1.4 |


| $\min$ | 6.5 | 6.5 | 6.1 | 6.5 | 6.3 | 6.2 | 6.1 | 6.3 | 6.5 | 6.7 | 6.6 | 6.6 | 6.8 | 6.7 | 6.7 | 6.7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| aver | 6.93 | 6.87 | 6.66 | 6.72 | 6.63 | 6.55 | 6.53 | 6.79 | 6.86 | 6.98 | 7.01 | 7.06 | 7.06 | 7.17 | 7.15 | 7.20 |
| $\max$ | 7.6 | 7.6 | 7.1 | 7.2 | 6.9 | 6.9 | 6.9 | 7.2 | 7.2 | 7.2 | 7.4 | 7.5 | 7.3 | 7.6 | 7.5 | 7.6 |
| $\mathbf{S}$ | 0.28 | 0.28 | 0.26 | 0.19 | 0.18 | 0.22 | 0.24 | 0.22 | 0.18 | 0.15 | 0.22 | 0.24 | 0.17 | 0.24 | 0.21 | 0.23 |



| Thickness，$m$ m | $\min$ | aver | $\max$ | S | n |
| :--- | :---: | :---: | :---: | :---: | :---: |
| The cylindrical part | 6.1 | 6.89 | 7.6 | 0.31 | 344 |



Fig．19．The map of the wall thickness of the specimen I3 in its original condition，mm．The diagram shows the position of the crack，resulting in the destruction of the specimen，the white dot indicated the start point of the destruction．Bold horizontal and vertical lines present mounted on the specimen strain gauges．All other designations as in Fig． 4.

Weight of empty specimen： 60.6 kgf ．Weight of the specimen filled with water： 92.5 kgf ．Water temperature： $23^{\circ} \mathrm{C}$ ．Weight of water： 31.9 kgf ．Internal volume of the specimen－31．9 liters．

Table 18. Strains $\left(\times 10^{3}\right)$, in the annular and axial directions, measured by strain gauges $1 \ldots 6$ mounted on the sample I3 ${ }^{1)}$.

| gage number |  | 1 | 2 | 3 | 4 | 5 | 6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Regulations |  | Defect | Defect | Defect | Defect | Tube | Tube |
| Direction |  | Ring | Ring | Axial | Axial | Ring | Ring |
| Step | P, MPa |  |  |  |  |  |  |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 | 2.12 | 0.367 | 0.367 | 0.092 | 0.092 | 0.110 | 0.110 |
| 2 | 3.13 | 0.541 | 0.495 | 0.128 | 0.138 | 0.156 | 0.165 |
| 3 | 3.84 | 0.679 | 0.633 | 0.165 | 0.165 | 0.202 | 0.211 |
| 4 | 5.05 | 0.926 | 0.899 | 0.211 | 0.220 | 0.266 | 0.275 |
| 5 | 5.93 | 1.164 | 1.073 | 0.257 | 0.257 | 0.312 | 0.321 |

${ }^{1)}$ The measurements were performed before the installation of the bandage.


Fig. 21. Strains measured by gauges 1 ... 6 .


Fig. 22. Sample I3: a - pipe section \#6 with defect; b-defect; c-sample I3 with a bandage.
The average remaining wall thickness in the defect -2.82 mm , average wall thickness around the defect -6.46 mm . After destruction, the average thickness of the wall around the defect and in the defect has not changed. The length of the weld along the axis of the tube is about 10 mm .

In order to align the outer surface of the pipe the cavity of the defect before installation of the bandage was filled with blend consisting of chopped to pieces roving (pieces of about 15 mm length) mixed with epoxy binder of cold hardening ("Himkontakt - Epoxy" TU-U 24.6-2558309112-006-2006).


Fig. 23. Installation of strain gauges in the defect (a) on the tube (b); roving for preparation the filling (c); defect filled with bland (d).


Fig. 24. Installation of strain gages on the bandage: a - in the area of the defect; b - in the regular part.

Strain gages, mounted on a bandage, were located over the strain gauges mounted on a metal pipe.

The bandage on the sample I3 consisted of 16 layers. Step of bandage winding $-2.36 \mathrm{~mm} /$ turn, the tension of the roving during bandage winding $\sim 4.6 \mathrm{kgf}$. General thickness of the bandage
$\sim 6.22 \mathrm{~mm}$. The width of the bandage $\sim 263 \mathrm{~mm}$, excluding a bevel on one side $\sim 234 \mathrm{~mm}$. Bandage is located between the 9th and 15th sections.

Table 19. Temperature during polymerization of the bandage.

| Day | Heating | Excerpt |
| :---: | :---: | :---: |
|  | from-to, ${ }^{\circ} \mathrm{C} / \mathrm{min}$ | ${ }^{\circ} \mathrm{C} / \mathrm{min}$ |
| 1 | $20-120 / 90$ | $120 / 120$ |
| 2 | $20-130 / 90$ | $130 / 90$ |
| 2 | $130-140 / 30$ | $140 / 180$ |
| 3 | $20-150 / 90$ | $150 / 180$ |

Table 20. Strains $\left(\times 10^{3}\right)$, measured by strain gauges $1 \ldots 6$ mounted on a metal area and $1 * \ldots 6^{*}$ - on bandaze ${ }^{11}$.

| Step | P, <br> MPa | 1 | 2 | 3 | 4 | 5 | 6 | $1^{*}$ | $2^{*}$ | $3^{*}$ | $4^{*}$ | $5^{*}$ | $6^{*}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 0 | 0.00 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | - |
| 1 | 3.13 | 0.532 | 0.541 | 0.128 | 0.147 | 0.165 | 0.147 | 0.128 | 0.101 | 0.156 | 0.046 | 0.138 | - |
| 2 | 5.35 | 0.770 | 0.807 | 0.220 | 0.202 | 0.275 | 0.257 | 0.330 | 0.293 | 0.238 | 0.110 | 0.229 | - |
| 3 | 6.40 | 0.899 | 0.935 | 0.275 | 0.229 | 0.330 | 0.312 | 0.422 | 0.385 | 0.275 | 0.138 | 0.266 | - |
| 4 | 7.53 | 1.027 | 1.054 | 0.321 | 0.266 | 0.385 | 0.367 | 0.513 | 0.477 | 0.330 | 0.193 | 0.321 | - |
| 5 | 8.99 | 1.210 | 1.201 | 0.403 | 0.312 | 0.468 | 0.449 | 0.706 | 0.651 | 0.403 | 0.266 | 0.376 | - |
| 6 | 10.36 | 1.375 | 1.357 | 0.523 | 0.358 | 0.523 | 0.513 | 0.990 | 0.917 | 0.513 | 0.358 | 0.431 | - |
| 7 | 12.92 | 1.568 | 1.540 | 0.752 | 0.440 | 0.651 | 0.642 | 1.632 | 1.495 | 0.770 | 0.477 | 0.532 | - |
| 8 | 14.69 | 1.605 | 1.770 | 0.908 | 0.972 | 0.743 | 0.734 | 2.127 | 1.962 | - | - | 0.605 | - |
| 9 | 16.65 | 1.944 | 2.274 | 1.091 | 1.229 | 0.844 | 0.844 | 2.677 | 2.494 | - | - | 0.688 | - |
| 10 | 18.38 | 2.613 | 2.934 | 1.302 | 1.495 | 0.954 | 0.963 | 3.182 | 2.998 | - | - | 0.770 | - |
| 11 | 19.90 | 3.237 | 3.952 | 1.595 | 1.742 | 1.064 | 1.036 | 3.613 | 3.393 | - | - | 0.889 | - |
| 12 | 20.65 | 3.897 | - | 1.953 | 2.054 | 1.164 | 1.128 | 3.787 | 3.585 | - | - | 0.963 | - |
| 13 | 21.21 | 4.447 | - | 2.219 | 2.375 | 1.265 | 1.220 | 3.961 | 3.732 | - | - | 0.981 | - |

${ }^{1)}$ The measurements were performed after installation of the bandage. Strain gages $1^{*} \ldots 6^{*}$ installed on the bandage over the strain gages $1 \ldots 6$.


Fig. 25. Strain measured by gauges $1 \ldots 6$ mounted on a metal area and $1^{*} \ldots 6^{*}$ on the bandage.

Table 21. Changes in weight of the specimen I3.

| after step | P, MPa | Weight G, kgf | $\Delta \mathrm{G}, \mathrm{g}$ |
| :---: | :---: | :---: | :---: |
| 0 | 0 | $96.2^{*}$ | 0 |
| 13 | 12.21 | $96.5^{*}$ |  |
| 13 | 21.21 | 96.4 | 300 |
| 14 | 22.76 | 96.7 | 600 |
| 15 | 24.81 | 97.2 | 1100 |
| 16 | 26.74 | 97.85 | 1750 |
| 17 | 27.90 | 98.65 | 2550 |
| 18 | 29.03 | - | - |

Notes: * - Weight with bandage and strain gauges. Further, without strain gages. The water temperature during the test $23^{\circ} \mathrm{C}$.


Fig. 26. Stages of internal pressure loading of the sample I3.
$P_{w}, P_{h}$ - work and test pressure; $P_{y}$ - yield pressure; $P_{b}, P_{b}^{*}$ - the maximum pressure that sustained the specimen and the pressure at which the failure occurred; 2 receivers - the pressure in the two paired receivers connected with the specimen.


| Thickness, $m m$ | $\min$ | aver | $\max$ | S | n |
| :--- | :---: | :---: | :---: | :---: | :---: |
| The cylindrical part | 5.1 | 6.47 | 7.5 | 0.46 | 344 |



Fig. 27. The map of the wall thickness of the sample after the destruction, mm. The diagram shows the position of the crack, resulting in the destruction of the sample, the white dot indicates the beginning of the destruction. Bold horizontal and vertical lines present ring and axial strain gauges. All other designations as in Fig. 4.

The nature of the destruction of the metal sample was plastic. Wall thickness at the area of fracture, measured with a caliper $\sim 4.5 \mathrm{~mm}$. The maximum crack opening $\sim 35.5 \mathrm{~mm}$. Crack length $\sim 280 \mathrm{~mm}$. After cutting the band in an axial direction and separation it from the metal pipe the gap between cut ends of the bandage $\sim 4 \mathrm{~mm}$.


Fig. 28. Defect section contour in the circumferential direction after the destruction of the sample I3.


Fig. 29. Specimen I3 after the destruction:
a sample after the test; b - in the process of disclosure of the defect; c - after the complete opening of the defect; d - filling of the defect; e - the cut area of the defect.

## Protocol of specimen I4 (bandage, no defects)

Loading of the specimen by internal pressure was done stepwise, after each step the pressure was released to 0 .

The chronology of measurements and loading of the sample by internal pressure is given below:

- stage $1 \ldots 7$ - measurement of change of the specimen volume prior to the plastic deformation (without bandage) in the water jacket;
- stage 1...5-measurement of deformations on the surface of the pipe by strain gauges (without bandage);
- installation of the bandage;
- stage $1 \ldots 6$ - measurement of deformation on the surface of the pipe and bandage by the strain gages;
- stage 1 ... 19 - - measurement of change of the specimen volume in the water jacket;
- stage 20 ... 26 - measurement of change of the bandage perimeter and of change of the specimen weight.

For the manufacture of the specimen was used the pipe section \# 5 with weight: 33.2 kgf .
Table 22. The length of the cylindrical portion of the specimen I4 and other axial dimensions in the original condition and after the destruction.

| \# | Linear size, mm | Sector |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | I | II | III | IV | average |
| In the initial state |  |  |  |  |  |  |
| 1 | length of the pipe piece, $1_{\text {o }}$ | 948,5 | 951 | 952 | 950 | 950,38 |
| 2 | length between sealing bottoms | 954 | 957 | 959 | 956 | 956,50 |
| 3 | distance between the sections I--III | 646 | 648 | 648,5 | 645 | 646,88 |
| 4 | distance between the sections I-II | 322 | 321,5 | 320 | 321,5 | 321,25 |
| 5 | distance between the sections II-III | 324 | 327,5 | 328 | 323,5 | 325,75 |
|  |  |  |  |  |  |  |
| After the destruction |  |  |  |  |  |  |
| 2 | length between sealing bottoms | 964 | 965 | 965 | 962 | 964,00 |
| 3 | distance between the sections I-III |  |  |  |  |  |
| 4 | distance between the sections I-II | 337,0 | 325,5 | 324,0 | 325,5 | 328,00 |
| 5 | distance between the sections II-III | 326,5 | 329 | 330 | 325,5 | 327,75 |

Note: The measurements were done in the middle of the sectors I ... IV, (Fig. 1). The distance between the cross sections was determined by the punched points. The distances between the sections I-II after the destruction was measured along the bulging surface.

Table 23. Specimen I4 perimeter before $\left(\mathrm{P}_{\mathrm{H}}\right)$ and after destruction $\left(\mathrm{P}_{\mathrm{K}}\right)$.

| Cross section $\rightarrow$ | I | II | III | average | Sec. 7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Perimeter, $\mathrm{P}_{\mathrm{H}}, \mathrm{mm}$ | 693,2 | 692,8 | 693 | 693,00 | 692,9 |
| Perimeter, $\mathrm{P}_{\mathrm{K}}, \mathrm{mm}$ | 700,5 | 703,0 | 700,5 | 701,33 | 759 |

Note: For the designation of sections see. Fig. 1.

Table 24. Distances between points of measure in initial state $\left(l_{\mathrm{H}}\right)$ and after fracture $\left(l_{\mathrm{K}}\right),(\mathrm{mm})$.

| Distance | Measuring <br> point \# | Sec. I |  | Sec. II |  | Sec. III |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{l}_{\mathrm{K}}$ | $\mathrm{l}_{\mathrm{H}}$ | $\mathrm{l}_{\mathrm{K}}$ | $\mathrm{l}_{\mathrm{H}}$ | $1_{\mathrm{K}}$ |  |
| $1^{*}-2^{*}$ | 1 | 42.6 | 42.8 | 42.8 | 43.5 | 42.8 | 43.0 |
| $2^{*}-3^{*}$ | 2 | 43.7 | 44.5 | 43.3 | 43.8 | 44 | 45.0 |
| $3^{*}-4^{*}$ | 3 | 44.2 | 44.8 | 43.4 | 44.0 | 44 | 44.6 |
| $4^{*}-5^{*}$ | 4 | 42.6 | 43.0 | 43 | 43.8 | 43 | 43.5 |
| $5^{*} 6^{*}$ | 5 | 42.2 | 42.6 | 43 | 43.5 | 43 | 43.6 |
| $6^{*}-7^{*}$ | 6 | 43.6 | 44.0 | 44.8 | 45.0 | 43.5 | 44.0 |
| $7^{*}-8^{*}$ | 7 | 44.6 | 45.0 | 45 | 45.8 | 44.3 | 45.0 |
| $8^{*}-9^{*}$ | 8 | 42.4 | 42.8 | 42.5 | 43.0 | 42.8 | 43.4 |
| $9^{*}-10^{*}$ | 9 | 42.5 | 43.2 | 42.8 | 43.4 | 42.6 | 42.8 |
| $10^{*}-11^{*}$ | 10 | 44.7 | 45.0 | 43.3 | 43.6 | 42.4 | 42.6 |
| $11^{*}-12^{*}$ | 11 | 44.5 | 44.8 | 43.5 | 44.0 | 42 | 42.2 |
| $12^{*}-13^{*}$ | 12 | 42.2 | 42.6 | 42.5 | 43.0 | 42.8 | 43.0 |
| $13^{*}-14^{*}$ | 13 | 43.2 | 43.6 | 42.8 | 43.2 | 43.2 | 44.0 |
| $14^{*}-15^{*}$ | 14 | 43.6 | 44.0 | 43.6 | 44.0 | 44.2 | 44.4 |
| $15^{*}-16^{*}$ | 15 | 44 | 44.6 | 43 | 43.8 | 44.8 | 45.2 |
| $16^{*}-1^{*}$ | 16 | 42 | 42.8 | 42.8 | 43.4 | 43 | 43.6 |
| $\Sigma$ | - | 692.6 | 700.1 | 692.1 | 700.8 | 692.4 | 699.9 |
| average | - | 43.29 | 43.76 | 43.26 | 43.80 | 43.28 | 43.74 |

Note: For the designation of sections see. Fig. 1.

|  |  | Thickness in original state |  |  |  |  |  |  |  |  |  |  |  | Sample |  |  | I4 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | II |  |  |  | III |  |  |  | IV |  |  |  |  |
|  | 1 | 6.2 | 6.3 | 6.0 | 6.3 | 6.5 | 6.6 | 6. | 6.9 | 6.8 | 6.8 | 6.8 | 7.4 | 7.0 | 6.7 | 6.1 |  | 6.4 |
|  | 2 | 6.4 | 6.3 | 6.0 |  | 6.2 | 6.5 | 6.8 | 6.8 | 7.0 | 7.0 | 7.2 | 7.1 | 6.7 | 6.5 | 6.1 |  | 6.1 |
|  | 3 | 6.3 | 6.4 | 5.9 |  | rack |  | 6.8 | 6.8 | 7.2 | 7.2 | 7.3 | 7.3 | 6.9 | 6.4 | 6.2 |  | 6.2 |
| I | 4 | 6.6 | 6.4 |  |  | 6.2 | 6.5 | 6.6 | 6.7 | 7.1 | 7.1 | 7.1 | 7.0 | 6.7 | 6.5 | 6.0 |  | 6.4 |
|  | 5 | 6. | 6.3 | 5 | 5.9 | 5.9 | 6.4 | 6.7 | 6.6 | 6.9 | 7.0 | 7.0 | 7.1 | 6.7 | 6.6 | 6.4 | 46 | 6.5 |
|  | 6 | 6.4 | 6.1 | 5.8 | 5.9 | 6.1 | 6.5 | 6.9 | 6.5 | 6.7 | 6.9 | 7.0 | 7.0 | 6.7 | 6.8 | 6.5 | 56 | 6.5 |
|  | 7 | 6.3 | 6.206 .0 |  | 6.2 | 6.3 | 6.9 | 6.8 | 6.5 | 6.7 | 6.7 | 6.9 | 6.9 | 6.7 | 6.8 | 6.5 | 5 | 6.4 |
|  | 8 | 6.4 | 6.1 | 6.1 | 6.2 | 6.5 | 6.7 | 6.8 | 6.6 | 6.6 | 6.7 | 7.0 | 7.1 | 6.8 | 6.5 | 6.5 |  | 6.3 |
|  | 9 | 6.5 |  | 6．2 | ． 4 | S． 4 | 6.8 | 6.6 | 6.4 | 6.5 | 6. | 7.2 | 6.8 | 6.4 | 6.4 | 5.3 | 36 | 6.3 |
|  | 10 |  | 2 | 6.319 |  |  |  | ＋13 | ． |  | 1 | ． 3 | 6.9 |  | 52 | 15.4 | 46 | 6.4 |
|  | 11 | 64 | 6.15 | 5.96 .1 |  |  |  |  |  |  |  |  | 6.8 |  |  |  |  |  |
| II | 12 | $\begin{aligned} & 60 \\ & 6.7^{1} \end{aligned}$ | $\begin{aligned} & 5.96 \\ & 5.95 \end{aligned}$ | $\begin{aligned} & 6.06 .0 \\ & 5.926 .0 \end{aligned}$ |  |  |  | $\begin{aligned} & 56.6 \\ & 4 \quad 6.5 \end{aligned}$ |  |  |  |  |  | 6.060 .26 .50 |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 14 |  | $59$ |  |  |  | $\begin{aligned} & 9{ }^{6}{ }^{6}\left(14^{5}\right)^{9} \\ & 1 \end{aligned}$ |  | $\begin{array}{r} 66.56 .6 \\ +6.56 .6 \end{array}$ |  |  |  | 6.96 .7 |  |  |  | 6.6 |  |  |
|  | 15 |  |  |  |  |  |  |  |  |  |  |  |  |  | 6.4 |
|  | 16 |  | 1.165 .9 |  |  | 5.96 .5 | 6.7 | 6.5 |  |  | $\begin{array}{lll}6.6 & 6.7\end{array}$ |  | 6.8 | 7.1 | 7.0 | 612＊ 18 ）． 7 |  |  | 6.5 |  | 6.5 |
|  | 17 |  | 6.2 | 6.2 | 26.4 | 6.7 | 6.4 | 6.56 .4 |  | $\begin{aligned} & 7.0 \\ & 6.9 \end{aligned}$ | $\begin{aligned} & 7.0 \\ & 7.3 \end{aligned}$ | $\begin{aligned} & 7.0 \\ & 6.8 \end{aligned}$ | $\begin{aligned} & 6.7 \\ & 6.8 \end{aligned}$ | 6.7 | 6.4 | 6.56 .4 |  |  |
|  | 18 | 6.2 | 6.2 | 6.2 | 6.3 | 6.4 | 6.9 | 6.36 .3 |  |  |  |  |  |  | 6.5 | 6.4 |  | 6.2 |
| III | 19 | 6.5 | 6.2 | 6.2 | 26.5 | 6.5 | 6.3 | 6.46 .5 |  | 7.2 | 7.2 | 6.8 | 6.6 | $\begin{aligned} & 6.3 \\ & 6.3 \end{aligned}$ | 6.5 | $6.8$ |  | 6.3 |
|  | 20 | 6.3 | 6.2 | 6.0 | 0.4 | 6.7 | 6.5 | 6.86 .9 |  | 7.1 | 7.2 | 7.0 | 6.5 |  |  |  |  |  |
|  | 21 | 6.2 | 5.9 | 6.1 | 6.0 | 6.3 | 6.6 | 6.76 .7 |  |  | $\begin{array}{ll}7.1 & 7.0\end{array}$ | 6.86.8 | 6.4 | $\begin{aligned} & 6.3 \\ & 6.4 \end{aligned}$ | 6.9 | $\begin{array}{ll}6.5 & 6.5 \\ 6.7 & 6.2 \\ 6.7 & 6.4\end{array}$ |  |  |
|  | 22 | 6.36 .2 |  | 6.16 |  | 6.3 | 6.5 | 6.7 | 6.7 | 7.1 | 7.0 |  | 6.6 | 6.76 | 6.9 | 6.76 .4 |  |  |


| 系 | 边 | 厌 | $\cdots$ | $\begin{array}{\|c\|} \hline \text { dav } \\ \hline \% \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: |
| 6 | 6.59 | 7.4 | 0.37 | 0.7 |
| 6 | 6.55 | 7.2 | 0.40 | 0.0 |
| 5.9 | 6.60 | 7.3 | 0.47 | 0.8 |
| 5.8 | 6.54 | 7.1 | 0.42 | －0．2 |
| 5.9 | 6.53 | 7.1 | 0.39 | －0．2 |
| 5.8 | 6.52 | 7 | 0.38 | －0．4 |
| 6 | 6.55 | 6.9 | 0.29 | 0.0 |
| 6.1 | 6.56 | 7.1 | 0.29 | 0.1 |
| 6.2 | 6.53 | 7.2 | 0.27 | －0．3 |
| 6.2 | 6.58 | 7.3 | 0.34 | 0.5 |
| 5.9 | 6.51 | 7.3 | 0.39 | －0．6 |
| 5.9 | 6.54 | 7.2 | 0.39 | －0．1 |
| 5.9 | 6.55 | 7.2 | 0.39 | 0.0 |
| 5.9 | 6.51 | 7 | 0.34 | －0．5 |
| 5.7 | 6.52 | 7 | 0.37 | －0．4 |
| 5.9 | 6.56 | 7.1 | 0.34 | 0.2 |
| 6.2 | 6.54 | 7 | 0.28 | －0．1 |
| 6.2 | 6.52 | 7.3 | 0.33 | －0．4 |
| 6.2 | 6.55 | 7.2 | 0.31 | 0.0 |
| 6 | 6.61 | 7.2 | 0.34 | 0.9 |
| 5.9 | 6.50 | 7.1 | 0.37 | －0．7 |
| 6.1 | 6.59 | 7.1 | 0.29 | 0.6 |


| $\min$ | 6.1 | 5.9 | 5.7 | 5.8 | 5.9 | 6.3 | 6.3 | 6.3 | 6.6 | 6.7 | 6.8 | 6.4 | 6.3 | 6.2 | 6 | 6.1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cp. | 6.38 | 6.14 | 6.01 | 6.17 | 6.38 | 6.55 | 6.62 | 6.63 | 6.92 | 7.04 | 7.00 | 6.86 | 6.63 | 6.57 | 6.45 | 6.39 |
| $\max$ | 6.7 | 6.4 | 6.3 | 6.5 | 6.7 | 6.9 | 6.9 | 6.9 | 7.2 | 7.3 | 7.3 | 7.4 | 7 | 6.9 | 6.8 | 6.7 |
| $\sigma$ | 0.16 | 0.16 | 0.15 | 0.21 | 0.20 | 0.16 | 0.16 | 0.16 | 0.19 | 0.19 | 0.16 | 0.25 | 0.19 | 0.19 | 0.22 | 0.14 |



| Thickness， mm | $\min$ | aver | $\max$ | S | n |
| :--- | :---: | :---: | :---: | :---: | :---: |
| The cylindrical part | 5.7 | 6.55 | 7.4 | 0.35 | 352 |


$\square$
thickness，mm samhle

Fig．30．The wall thickness of the specimen in its original condition，mm．
The cross－section II is between the 11th and the 12th lines，but for measurement of its thickness was taken the 12 line．An asterisk $\left(^{*}\right.$ ）marks gages glued to the bandage．All other designations as in Fig． 4．The diagram shows the position of the crack，resulted in the destruction of the specimen．The white dot indicates the start point of the destruction．By bold horizontal and vertical lines are presented the strain gauges installed on the specimen surface．


Fig. 31.Specimen I4 before the installation of the bandage.
a - general view of the specimen; b - piece of the pipe welded to the sealing bottom to fixing the specimen in the jig of the machine; c - weld of top sealing bottom; d - nuts welded to sealing bottom for fixing specimen in the tailstock of the machine; e - weld of the lower bottom.

Weight of empty specimen: 61.8 kgf . Weight of the specimen filled with water: 93.6 kgf . Water temperature: $10{ }^{\circ} \mathrm{C}$. Weight of water: 31.8 kgf . Internal volume of the specimen of 31.8 liters. Weight of the bandage -3.6 kgf ; general weight of installed strain gauges and connecting wires -0.1 kgf . Length of the sealing weld along the axis of the pipe -10 mm .

Table 25. Perimeters of the cross-sections in specimen original state - $\mathrm{P}_{\mathrm{H}}$, during the test (after removing from the water jacket) - P and after the specimen destruction $-\mathrm{P}_{\mathrm{K}} \mathrm{mm}$.

|  |  | $\begin{gathered} \mathrm{P}, \\ \mathrm{MPa} \end{gathered}$ | Weight G, kgf | $\Delta \mathrm{G}$ | Perimeter, mm. |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section $\rightarrow$ |  |  |  |  | I | II | - | III | 7 | - |
| Before installing the bandage | $\mathrm{P}_{\mathrm{H}}$ |  |  |  | 693.2 | 692.8 |  | 693.0 | 692.9 |  |
| Section $\rightarrow$ |  |  |  |  | I* | II* | II** | III* | 7 | 7* |
| After installing the bandage |  | 0 | 97.3 |  | 709.2 | 712.8 | 708.4 | 710.8 | 692.9 | 708.8 |
| After step | 19 |  | $97.5^{1)}$ |  |  |  |  |  |  |  |
|  | 19 | 27.02 | 98.5 | 200 | 711.2 | 715.2 | 710.8 | 712.2 | 697.6 | 710.8 |
|  | 20 | 28.60 | 98.5 | 200 | 711.6 | 716.5 | 711.5 | 713.0 | 699.0 | 711.6 |
|  | 21 | 30.10 | 98.6 | 300 | 712.4 | 717.0 | 712.4 | 714.0 | 700.8 | 712.8 |
|  | 22 | 31.60 | 98.7 | 400 | 713.2 | 717.8 | 712.8 | 714.4 | 702.0 | 713.8 |
|  | 23 | 33.10 | 98.8 | 500 | 713.6 | 718.2 | 713.4 | 715.2 | 703.5 | 714.0 |
|  | 24 | 35.10 | 99.0 | 700 | 714.8 | 719.6 | 714.5 | 716.0 | 705.2 | 715.2 |
|  | 25 | 37.10 | 99.1 | 800 | 715.4 | 719.8 | 715.0 | 716.5 | 707.2 | 715.8 |
|  | 26 | 39.60 | - | - | 715.6 | 720.2 | 715.2 | 717.2 | 759 | - |
| The thickness of the ba (approximately) | dage, |  |  |  | 2.5 |  | 2.5 | - |  |  |
|  |  |  |  |  | I | II | - | III | 7 | - |
| After removing the bandage | $\mathrm{P}_{\mathrm{K}}$ |  |  |  | 700.5 | 703.0 |  | 700.5 | 759 |  |

Notes: Section I is located at a distance of 150 mm from the top of the pipe section, and in welded specimen at distance of 155 mm from the nearest bottom. Cross section II is located in the middle of the pipe section, and in welded specimen at a distance of 475 mm from the nearest bottom. Cross section III is located at a distance of 150 mm from the bottom of the pipe section, and in welded specimen at a distance of 155 mm from the nearest bottom. The cross-section 7 (7th from the top) located in the welded sample at a distance of 280 mm from the nearest bottom. 7* - section of the bandage corresponding to the cross section 7 of the pipe, but located 20 mm below the edge of the bandage. The sections marked with * relate to the bandage. Cross section II ** is shifted above the strain gage in axial direction. Width of roulette tape -10 mm ., its thickness -0.2 mm . The slot width -25 mm .
${ }^{1)}$ - here, unlike of other cases, weight does not include the fittings.

Table 26. Strains $\left(\times 10^{3}\right)$ by the gages installed on the bandage.

|  |  | gages |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | hoop direction |  |  |  |  |  |  |  | axial direction |  |  |  |
| Step | $\mathrm{P}, \mathrm{MPa}$ | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 |
| 1 | 3,68 | 0,269 | 0,215 | 0,296 | 0,153 | 0,242 | 0,251 | 0,188 | 0,265 | 0,063 | - | 0,054 | 0,054 |
| 2 | 6,56 | 0,476 | 0,404 | 0,520 | 0,292 | 0,431 | 0,458 | 0,332 | 0,467 | 0,117 | - | 0,099 | 0,099 |
| 3 | 8,52 | 0,619 | 0,529 | 0,682 | 0,377 | 0,547 | 0,583 | 0,440 | 0,610 | 0,153 | - | 0,126 | 0,126 |
| 4 | 11,85 | 0,843 | 0,745 | 0,933 | 0,538 | 0,772 | 0,817 | 0,619 | 0,852 | 0,215 | - | 0,179 | 0,179 |
| 5 | 12,57 | 0,897 | 0,803 | 1,000 | 0,583 | 0,812 | 0,875 | 0,664 | 0,906 | 0,229 | - | 0,188 | 0,188 |

Note: strain measurement was made after the preliminaryloading in the water jacket (after step 7).
Installation of the bandage: the tension of roving kgf $4.2 \pm 0,6$; step of wrapping along the axis of the specimen $-2.36 \mathrm{~mm} / \mathrm{turn}$; the number of layers -8 . Weight of the roving bobbin before winding - 6.68 kg , after winding - 3.80 kgf . The weight of the used roving - 2.88 kgf . Polymerization of the bandage: temperature $-120^{\circ} \mathrm{C}$, duration -20 hours. Polymerization was done in several shifts, each consisted of raising the temperature to $120^{\circ} \mathrm{C}$ and subsequent exposure for several hours.

After installing the bandage, it was cut in circumferential direction (at section 7) to form a groove with width -26 mm . The thickness of the carved out ring by according to 18 measurements.$2 \mathrm{~mm} \pm 2.5$. In order to remove the ring from the specimen an axial groove was done. The ring easily separated from the pipe. After removal of the ring the width of the axial groove increased by 3.2 mm .


Fig. 32. Axial groove in the ring (a); bandage after removal of the ring (b).


Fig. 33. Strain gages on the surface of the pipe before installing the bandage (a) and at the bandage surface (b).

Strain gages, mounted on a bandage, were placed over the strain gages on the surface of the pipe.

Table 27. Strain $\left(\times 10^{3}\right)$ by gauges after bandage installation

|  |  | gages |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ring direction |  |  |  |  |  |  |  | axial direction |  |  |  |
| Step | $\begin{gathered} \hline \mathrm{P}, \\ \mathrm{MPa} \end{gathered}$ | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 0 | 0 | - | 0 | - | 0 | - | - | 0 | - | 0 | - | - | 0 |
| 1 | 2.14 | - | 0.126 | - | 0.031 | - | - | 0.085 | - | 0.045 | - | - | 0.027 |
| 2 | 3.83 | - | 0.229 | - | 0.063 | - | - | 0.166 | - | 0.085 | - | - | 0.045 |
| 3 | 5.90 | - | 0.354 | - | 0.090 | - | - | 0.260 | - | 0.126 | - | - | 0.072 |
| 4 | 8.46 | - | 0.507 | - | 0.126 | - | - | 0.377 | - | 0.153 | - | - | 0.081 |
| 5 | 11.66 | - | 0.700 | - | 0.188 | - | - | 0.520 | - | 0.224 | - | - | 0.099 |
| 6 | 12.42 | - | 0.758 | - | 0.197 | - | - | 0.556 | - | 0.229 | - | - | 0.126 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Step | $\begin{gathered} \hline \mathrm{P}, \\ \mathrm{MPa} \end{gathered}$ | 1* | 2* | 3* | 4* | 5* | 6* | 7* | 8* | 9* | 10* | 11* | 12* |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 0 | 0 | 0 | 0 | - | 0 | - | - | 0 | - | 0 | - | - | 0 |
| 1 | 2.14 | 0.153 | 0.094 | - | 0.076 | - | - | 0.117 | - | 0.036 | - | - | 0.031 |
| 2 | 3.83 | 0.251 | 0.179 | - | 0.162 | - | - | 0.188 | - | 0.045 | - | - | 0.045 |
| 3 | 5.90 | 0.386 | 0.265 | - | 0.265 | - | - | 0.287 | - | 0.072 | - | - | 0.072 |
| 4 | 8.46 | 0.538 | 0.386 | - | 0.368 | - | - | 0.413 | - | 0.103 | - | - | 0.103 |
| 5 | 11.66 | 0.754 | 0.547 | - | 0.507 | - | - | 0.565 | - | 0.153 | - | - | 0.135 |
| 6 | 12.42 | 0.799 | 0.583 | - | 0.538 | - | - | 0.610 | - | 0.162 | - | - | 0.148 |

After removal of the specimen from the water jacket there were revealed small circular cracks around the bandage.

Table 28. Change in the volume of specimen I4 during test in the water jacket, (WJ). Steps 1 ... 19.

| Step \# | $\begin{aligned} & \mathrm{P}_{\max }, \\ & \mathrm{MPa} \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{P}_{\text {min }}, \\ & \mathrm{MPa} \end{aligned}$ | $\begin{aligned} & \Delta \mathrm{V}_{\mathrm{ti}}, \\ & \mathrm{~cm}^{3} \end{aligned}$ | $\begin{gathered} \Delta \mathrm{V}_{\mathrm{pi}}, \\ \mathrm{~cm}^{3} \end{gathered}$ | burette |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| without bandage |  |  |  |  |  |  |
| 0 | 0 | 0 | 0 | 0 | A |  |
| 1 | 3,85 | 3,85 | 21,926 | 0 | A |  |
| 2 | 5,68 | 5,66 | 32,295 | 0 | A |  |
| 3 | 6,58 | 6,57 | 37,440 | 0 | A | 野雨 |
| 4 | 7,69 | 7,68 | 43,851 | 0 | A |  |
| 5 | 8,78 | 8,76 | 50,025 | 0 | A |  |
| 6 | 10,50 | 10,49 | 59,999 | 0,1583 | A |  |
| 7 | 12,51 | 12,50 | 72,347 | 0,7915 | A | 4 -13075 |
|  |  |  |  |  |  |  |
| with bandage |  |  |  |  |  |  |
| 0 | 0 | 0 | 0 | 0 | A | - $\mathrm{V}^{\text {O }}$, |
| 1 | 1,24 | 1,24 | 6,015 | 0 | A | , |
| 2 | 3,05 | 3,04 | 14,881 | 0 | A | 10 |
| 3 | 4,88 | 3,86 | 23,983 | 0 | A | $1)$ |
| 4 | 6,81 | 6,79 | 33,561 | 0 | A | $\therefore$ - |
| 5 | 8,03 | 8,02 | 39,735 | 0 | A |  |
| 6 | 9,88 | 9,86 | 49,155 | 0 | A |  |
| 7 | 12,03 | 12,01 | 59,840 | 0 | A |  |
| 8 | 13,40 | 13,38 | 66,806 | 0 | A |  |
| 9 | 14,59 | 14,57 | 73,138 | 0 | A |  |
| 10 | 15,65 | 15,62 | 78,996 | 0 | A |  |
| 11 | 16,93 | 16,89 | 86,752 | 0,9498 | A |  |
| 12 | 18,90 | 18,83 | 101,000 | 4,7492 | A |  |
| 13 | 20,60 | 20,50 | 115,565 | 9,6568 | A |  |
| 14 | 21,43 | 21,32 | 119,522 | 8,7069 | A | Fig. 34. The water jacket |
| 15 | 22,80 |  | 146,277 | 26,4374 | A |  |
| 16 | 24,00 | 23,76 | 164,440 | 38,5298 | B |  |
| 17 | 25,00 | 24,70 | 173,384 | 38,5298 | B |  |
| 18 | 25,92 | 25,71 | 192,649 | 49,5384 | B |  |
| 19 | 27,02 | 26,74 | 201,594 | 49,5384 | B |  |

Note: $\Delta \mathrm{V}_{\mathrm{ti}}$ - the maximum (full) change of the volume at each step was determined at the end of exposure to max pressure; $\Delta \mathrm{V}_{\mathrm{pi}}$ - residual change of volume at the appropriate step after pressure release. Changing of the volume was determined by burettes of water jacket (Fig.34) as the difference between level of the liquid columns multiplied by a calibration coefficient and with the addition of $7.4 \%$ taking into account the error of the burette A , and $1.78 \%$ for burette B .


Fig. 35. Internal pressure loading of the specimen.
$P_{w}, P_{h}$ - working pressure and test pressure, accordingly; $P_{y}$ - yield pressure; $P_{b}, P_{b}^{*}$ - the maximum pressure that sustained the specimen and the pressure at which the failure occurred, accordingly; 2 receivers - the pressure in the two paired receivers connected without the specimen.

The length of the broken part of the bandage along the pipe axis $\sim 225 \mathrm{~mm}$. The maximum crack opening in the pipe -36.6 mm . The nature of the destruction of the metal sample was plastic. Wall thickness at the area of fracture, measured with a caliper $\sim 4.5 \mathrm{~mm}$. Crack length $\sim 280 \mathrm{~mm}$.

Table 29. The wall thickness of the specimen in sections $6,7,8$, after the destruction mm .

|  | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ | $\mathbf{9}$ | $\mathbf{1 0}$ | $\mathbf{1 1}$ | $\mathbf{1 2}$ | $\mathbf{1 3}$ | $\mathbf{1 4}$ | $\mathbf{1 5}$ | $\mathbf{1 6}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{6}$ | 6.1 | 5.6 | 5.3 | 5.4 | 5.7 | 6.3 | 6.6 | 6.4 | 6.5 | 6.8 | 6.9 | 7.0 | 6.5 | 6.6 | 6.4 | 6.2 |
| $\mathbf{7}$ | 5.8 | 5.4 | 5.0 | 5.1 | 5.8 | 6.4 | 6.4 | 6.1 | 6.2 | 6.5 | 6.5 | 6.6 | 6.2 | 6.3 | 5.9 | 5.8 |
| $\mathbf{8}$ | 5.7 | 5.5 | 5.5 | 5.6 | 6.0 | 6.4 | 6.3 | 6.0 | 6.2 | 6.4 | 6.7 | 6.7 | 6.4 | 6.1 | 6.0 | 5.7 |

Note: The wall thickness of cross-section in other cases has not changed significantly.


Fig. 36. Specimen (a) - after the destruction; (b, c) - after removal of the bandage.

## Summary results of the samples I1 ... I4 and material.

## Basic data about the pipe.

Pipe:
dimension - $219 \times 6$; material -20 steel (carbon steel; weight per meter $\sim 33.51 \mathrm{kgf}$.
Quality certificate \# 4/4050. The pipe is manufactured in accordance with GOST 8732-78; GOST 8731-74 Clause 1.2. B (with standardization of mechanical properties and chemical composition). Hot rolled seamless steel pipes. The manufacturer: OJSC "Interpipe NTRP plant." Party number 443, \# 32416 melt.

Table 30. The mechanical properties of the pipe material.

| According to | $\sigma_{\mathrm{B}}, \mathrm{MPa}$ <br> $\left(\mathrm{kgf} / \mathrm{mm}^{2}\right)$ | $\sigma_{02}, \mathrm{MPa}$ <br> $\left(\mathrm{kgf} / \mathrm{mm}^{2}\right)$ | $\delta_{5}, \%$ | Flattening |
| :--- | :---: | :---: | :---: | :---: |
| GOST 8731-74, clause 1.2. B. | $412(42)$ | $245(25)$ | 21 |  |
| Melt number 32416 | $475,78(48,5)$ | $323,73(33,0)$ | 32,0 | Satisfactorily |
|  | $480,69(49,0)$ | $328,64(33,5)$ | 33,0 | Satisfactorily |
| Circumferential direction $^{*}$ | 474,76 | 305 | 33,13 |  |
| Axial direction $^{*}$ | 461,40 | 314 | 40,97 |  |

- Data obtained at the Problems of Strength Institute by testing of the samples cut from the pipe.
$\sigma_{\mathrm{B}}$ - tensile strength, $\sigma_{02}$ - yield strength, $\delta_{5}$ - relative extension,

Table 31. Chemical composition of the pipe material.

| According to | Mass fraction of elements, \% |  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | C | Mn | Si | S | P | Cr | Ni | Cu |  |
| By GOST 1050-88 | $0.17-0.24$ | $0.35-0.65$ | $0.17-0.37$ | $<0.040$ | $<0.035$ | $<0.25$ | $<0.30$ | $<0.30$ |  |
| Melt \# 32416 $_{\text {Actually }^{*}}$ | 0.19 | 0.54 | 0.29 | 0.02 | 0.011 | 0.07 | 0.05 | 0.08 |  |
| ${ }^{*}$ | 0.177 | 0.55 | 0.289 | 0.018 | 0.008 | 0.078 | 0.065 | 0.070 |  |

- the data obtained in the laboratory of the Electric Welding Institute.

According to GOST 8732-78: wall thickness tolerance $+12.5 /-15.0 \%$; outer diameter tolerance $\pm 1,0 \%$; curvature of any portion of the pipe with length of 1 m should not exceed 1.5 mm .


Fig. 37. Tensile diagrams ( $\bar{\sigma}, \bar{e}$ ) of specimens cut in the hoop (R) and axial (A) direction from the pipe in the initial state, and built on their base the actual stress-strain diagram $\sigma_{i}, \varepsilon_{i}$.

At the figure also are shown calculated values of the limit state of the pipe under internal pressure, and the maximum intensity of the strain obtained during tests of samples I1 and I3.

## Basic data of the roving



Fig. 38. Effort $F_{1}$ per one roving thread (R) (tensile test of loop (L), consisting of a certain amount of roving threads).

## Base characteristics of specimens I1...I4

Table 32. The summary characteristics of the specimens I1 ... I4 «INNOPIPES».

| Parameter | UM. | sample ID |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | I1 | I2 | I3 | I4 |
| Pipe section |  |  |  |  |  |
| Outside diameter, $D_{O}$ | mm | 220,15 | 219,77 | 220,15 | 219,99 |
| will ${ }^{\text {a }}$ average, $s_{O}$ | mm | 6,73 | 6,76 | 6,89 | 6,55 |
| minimal, $s_{\text {min }}$ | mm | 5,9 | 6,1 | 6,1 | 5,7 |
| Internal volume, $W_{o}$ | 1 | 32 | 31,9 | 31,9 | 31,8 |
| Distance between the sealing bottoms, $l_{o}$ | mm | 953 | 953,25 | 954,5 | 956,5 |
| Yield pressure, $\left[P_{Y}\right]$ | MPa | 10,43 | - | - | 10,50 |
|  |  |  |  |  |  |
| Defect |  |  |  |  |  |
| Remaining wall ${ }^{\text {average, } t_{o}}$ | mm | - | 2,7 | 2,82 | - |
| thickness $\quad$ minimal, $t_{\text {min }}$ | mm | - | 2,4 | 2,3 | - |
| Linear dimensions (length $\times$ width) | mm | - | $\begin{gathered} 133 \times \\ 102 \end{gathered}$ | $\begin{gathered} \hline 133,2 \times \\ 102,2 \end{gathered}$ | - |
| Estimated coefficient of strength reduction |  |  | 0,499 | 0,493 |  |
| Yield pressure, $\left[P_{Y}\right]$ | MPa | - | 5,83 | 5,93 | - |
|  |  |  |  |  |  |
| Bandage |  |  |  |  |  |
| outer diameter, $D_{O^{*}}$ | mm | - | - | 232,59 | 225,02 |
| number of layers, $n$ | pcs | - | - | 16 | 8 |
| thickness, $s_{o *}$ | mm | - | - | 6,22 | 2,52 |
| thickness of layer, $\Delta r$ | mm | - | - | 0,389 | 0,315 |
| Step of winding, $\Delta l$ | $\begin{gathered} \mathrm{mm} / \\ \mathrm{rev} \end{gathered}$ | - | - | 2,36 | 2,36 |
| Yield pressure, $\left[P_{Y}\right]$ | MPa | - | - | 16,65 | 16,93 |
|  |  |  |  |  |  |
| According loading diagram |  |  |  |  |  |
| Yield pressure, $P_{Y}$ | MPa | 20 | - | 19,6 | 22,14 |
| Maximum pressure, $P_{b}$ | MPa | 27,59 | 13,83 | 29,06 | 39,65 |
| Pressure destruction, $P_{b}^{*}$ | MPa | 27,44 | 13,83 | 29,03 | 33,87 |
| The actual strength factor, $\varphi$ | - | 1 | 0,501 | 1,053 | 1,437 |

$\left[P_{Y}\right]$ - Yield pressure for samples I1 and I4 was determined by water jacket, for samples I2 and I3 by strain gages. $P_{Y}$ - Yield stress, determined by the internal pressure loading diagram.


Fig. 39. Internal pressure loading diagrams of specimens I1, I2, I3 and I4.
$P_{w}, P_{h}$ - working pressure and test pressure, correspondingly; $P_{y}$ - yield pressure; $P_{b}, P_{b}^{*}$ - the maximum pressure that sustained the specimen and the pressure at which the failure occurred, correspondingly; 2 receivers - the pressure in the two paired receivers connected without the specimen. Parabola - approximation equation of the second degree.


Fig. 40. Specimens I1, I2, I3 and I4 after the test.


() - Parameter for reference

Parameters of the samples

|  | 11 | 12 | 13 | 14 |
| :--- | :---: | :---: | :---: | :---: |
| $D_{0}, \mathrm{~mm}$ | 220,15 | 219,77 | 220,15 | 219,99 |
| so, mm | 6,73 | 6,76 | 6,89 | 6,55 |
| $l o, \mathrm{~mm}$ | 953 | 953,25 | 954,5 | 956,5 |
| to, mm | - | 2,7 | 2,82 | - |
| $a \times b, \mathrm{~mm}$ | - | $133 \times 102$ | $133,2 \times 102,2$ | - |
| $n, \Delta l \mathrm{~mm}$ | - | - | $16,2,36$ | $8,2,36$ |
| so ${ }^{*}, \mathrm{~mm}$ | - | - | 6,22 | 2,52 |
| $a 1, \mathrm{~mm}$ | - | - | 50 | $(l o-a) / 2$ |
| $a 2, \mathrm{~mm}$ | - | - | 25 | 0 |



Fig. 41. Specimen I3 scheme.

